

**COMPARATIVE GROUNDING CONNECTOR TEST**

**PERFORMED FOR**

**ERICO®, INC.**

**SOLON, OHIO**

**PROJECT NUMBER C94901**

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**Southern Development** 

*a subsidiary of The Southern Company*

**COMPARATIVE GROUNDING CONNECTOR TEST**


**PERFORMED FOR**

**ERICO®, INC.**

**SOLON, OHIO**

**PROJECT NUMBER C94901**

REQUESTED BY: MR. CURT STIDHAM  
ERICO, INC.

PROJECT MANAGER:   
T. L. McKoon

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## Comparative Grounding Connector Test

Performed For

ERICO®, Inc.

Solon, Ohio

Project # C94901

### **INTRODUCTION**

Mr. Curt Stidham, of ERICO®, Inc., contracted with Southern Electric International (SEI)/Georgia Power Research Center to evaluate three different designs of direct burial, electrical grounding connectors. The three designs chosen were exothermically welded (Cadweld®), bolted wedge, and die compression type connections. Mr. Stidham was interested in the heat rise performance characteristics of the various connections when installed on 250 kcmil, 37 strand, soft drawn copper conductor. The conductors were artificially aged in an oven for 24 hours at 500°F to simulate oxidized conductors in an existing ground grid system.

Ten connectors were included in the test program; they are as follows.

- Two exothermically welded type connectors, (Cadweld® Part Number TAC2V2V)
- Two bolted wedge type connectors (AMP, Inc. Part Number 81228-1)
- Two die compression, cross connectors (Burndy Part Number YGL29C29)
- Two die compression, tap connectors (Burndy Part Number YGHC29C29)
- Two die compression, cross connectors (T & B Part Number GG40250-40250)

A complete description and photographs of the connectors tested are included in the **SAMPLES TESTED** section of this report.

The test was conducted to the IEEE Std. 837-1989, "IEEE Standard for Qualifying Permanent Connections Used in Substation Grounding", Section 8.2.1 through 8.7.3, "Current Temperature Cycling", with the following exceptions:

- 8.2.2 Test Samples.....Two samples of each connector type were tested, rather than four as directed by the standard.

- **8.5.1 Current Cycling Period.....**The IEEE Std. 837-1989 calls for, as part of section 8 (Current-Temperature Cycling), a minimum temperature of 350°C (8.5.1) for copper conductor. This test program conducted current-temperature cycles to a control conductor temperature of 550°C. Referencing ANSI/IEEE Std. 80-1986, the fusing temperature of soft drawn copper wire is 1083°C, thus the minimum temperature required in IEEE Std. 837-1989 for Current-Temperature Cycling represents only 32% of the fusing temperature. Increasing the testing temperature to 550°C represents a temperature that is 51% of the fusing temperature, thereby providing a harsher test condition on the ability of grounding connectors to surpass the performance requirements of IEEE Std. 837-1989.
- **8.5.2 Number of Cycles.....**The IEEE Std. 837-1989 calls for, as part of Section 8 (Current-Temperature Cycling), a minimum of 25 current temperature cycles (8.5.2) This test program conducted 100 current-temperature cycles to provide data on the margins with which the grounding connectors could surpass this minimum requirement.
- **8.7 Measurements.....**Temperature measurements were made at the end of each of the 100 cycles rather than every five cycles as directed by the standard. Resistance measurements were made every tenth cycle, through cycle 100, rather than every five cycles as directed by the standard.
- **NOTE:** Aged cable was chosen for the test to simulate a common situation that exists when a new connection must be made to an existing ground grid network. The grid conductors, over years of service, will become oxidized and wire brushing the exterior of the cable, before the installation of a grounding connector, will not remove the oxide between the interior strands. Therefore, the resulting connector resistance will most likely be higher than an equivalent connection made to pristine conductor. Therefore, the use of aged conductor provided results on connector performance of a practical service condition that is not addressed in IEEE Std. 837-1989, Section 8. All test conductors were serviced aged by heating in an oven for 24 hours at a temperature of 500°F prior to installing the grounding connectors.
- Pages 13 and 14 of IEEE Std.837-1989 are included in **APPENDIX 2.**

## SUMMARY

A modified IEEE Std. 837-1989, Current-Temperature Cycle Test (Section 8) was performed on a variety of electrical grounding connectors to evaluate their relative performance. The connection styles evaluated were those typically used to join a ground lead to a grid system, or to make a connection within the system itself. The test was modified from the standard to produce harsher testing conditions and provide more meaningful results. Instead of clean new conductor, the test was performed on oxidized conductor to simulate conditions found in making connections to existing grids. Also, the control conductor soak temperature was increased from 350°C to 550°C. Current-Temperature Cycle testing was carried out for 100 cycles to provide a more realistic performance comparison.

Results of the test show that the exothermically welded (Cadweld®) connectors, Part Number TAC2V2V out performed the bolted wedge, AMP Part Number 81228-1, and die compression, Burndy Part Numbers YCL29C29 and YGHC29C29, and Thomas and Betts Part Number GG40250-40250 connectors by a wide margin.

By the conclusion of the first cycle all the connectors tested, except the Cadweld® welded connectors, had exceeded the control conductor temperature of 550°C and failed the maximum temperature requirement of IEEE Std. 837-1989 (Section 5.3.1). At this point, both of the exothermically welded (Cadweld®) connectors were still operating at a temperature well below that of the control conductor. The test was continued until either the connector or the conductor burned through and caused an open circuit in the test loop. When an open circuit occurred, the connector was shunted and the test was allowed to continue.

By the conclusion of the 21st cycle all the connectors tested, except for the Cadweld® welded connectors and the Burndy #2 tap connector (Part Number YGHC29C29), had to be shunted. The remaining Burndy connector lasted through cycle 34. At this point, both of the Cadweld® welded connectors were operating at a temperature well below that of the control conductor.

At the end of cycle 58, the Cadweld® welded connector #2 had exceeded the control conductor temperature. The Cadweld® welded connector had to be shunted before the start of the 65th cycle due to the conductor fusing on the 64th cycle, at a distance of approximately eight inches away from the connector. The Cadweld® welded connector #1 lasted through the entire 100 cycles without its temperature ever exceeding that of the control conductor.

Graphs detailing each connector's performance are included in APPENDIX 1. Charts of each connector's temperature, at each operable cycle, up to 100 cycles, are included in the TEST PROGRAM section.

## **SAMPLES TESTED**

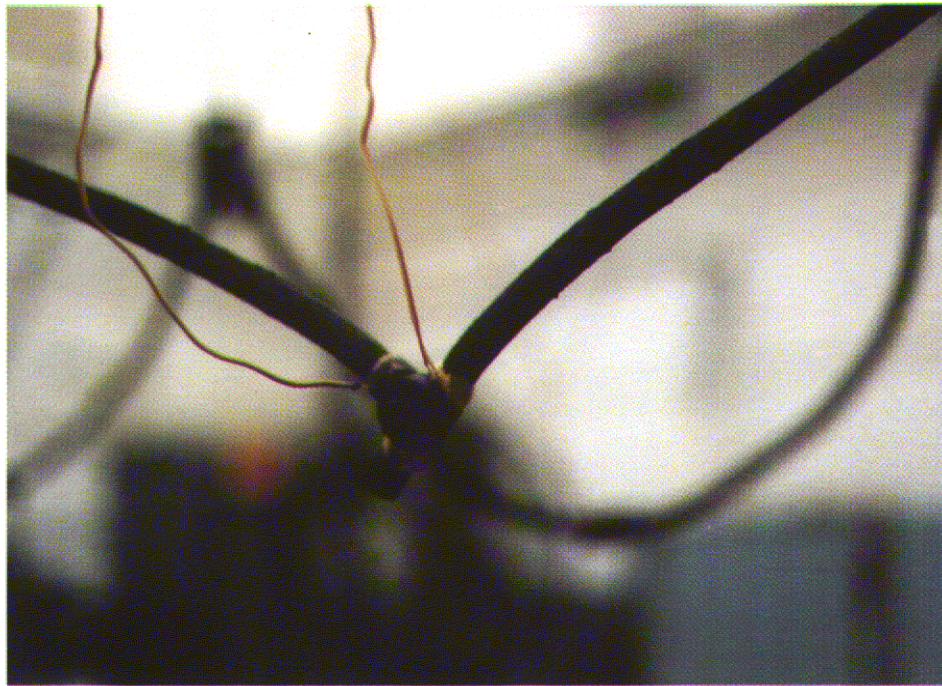
ERICO®, Inc., in Solon, Ohio, provided the molds and weld materials to install the horizontal Tee (Part Number TAC2V2V), cable to cable, exothermically welded connections. The bolted wedge and die compression type connectors were chosen by ERICO®, Inc., and the Georgia Power Research Center procured the connectors from various manufacturers, along with the proper dies used for installation. No dies or compression tools were required to install the bolted wedge connectors.

The conductor used for the test program was 250 kcmil, 37 strand, soft drawn copper, of the same type and size commonly used in typical substation ground grids. The conductor was artificially serviced aged, by exposure to 500°F for 24 hours in an oven, prior to installing the connectors. For all connectors, prior to connector installation, the conductor ends, and circumference at the ends, were wire brushed to remove any oxide build up caused by the service aging.

**FIGURES 1 & 2** are photographs of Cadweld® exothermically welded connections #1 and #2 taken during the 100 cycle, current cycle, heat rise test.



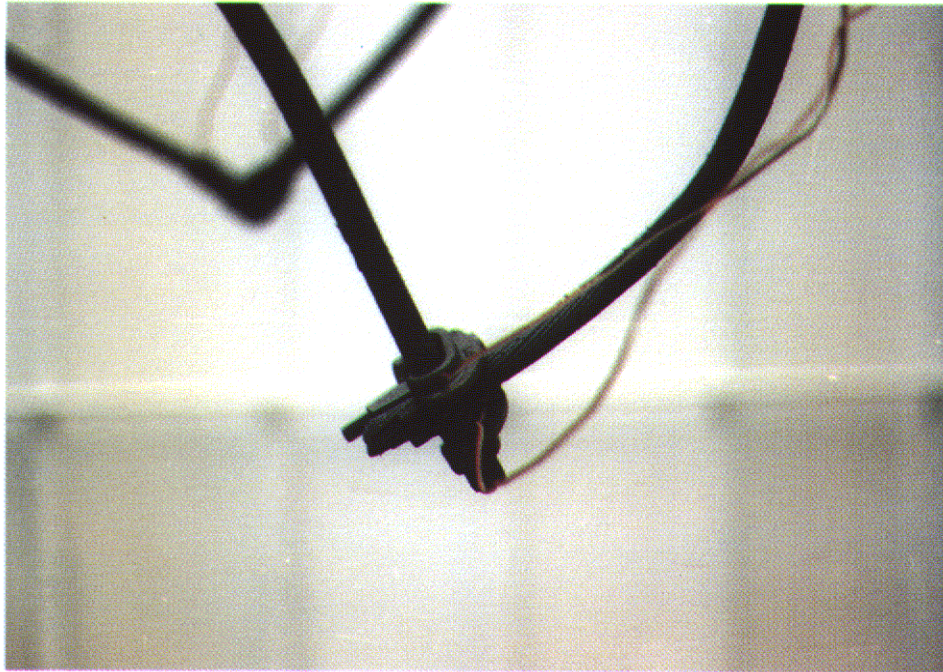
**FIGURE 1**  
Cadweld® exothermically welded connection #1  
Page (4)



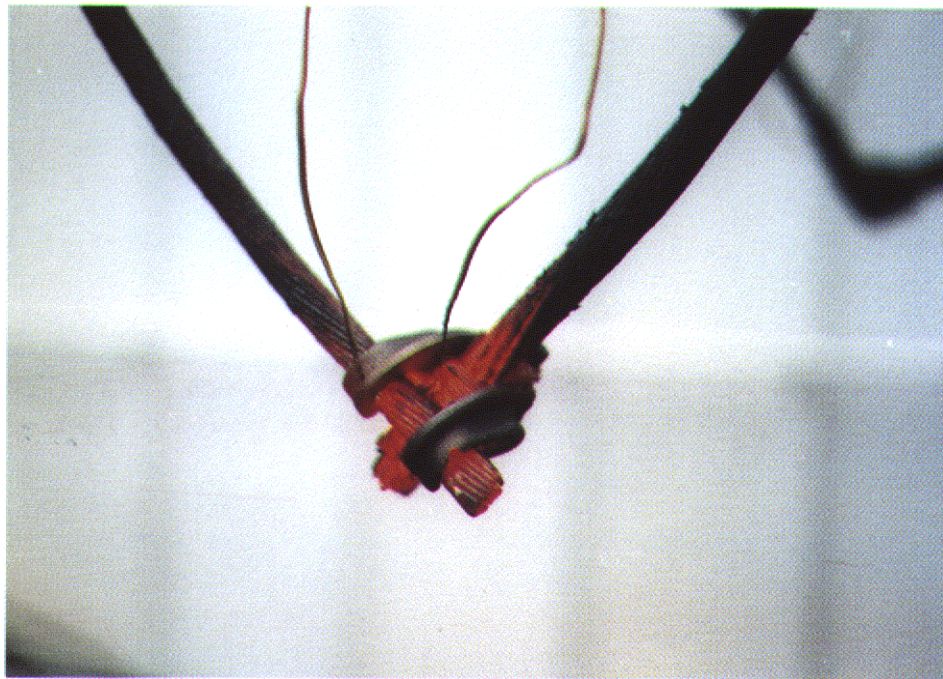
**FIGURE 2**  
Cadweld® exothermically welded connection #2  
Photograph taken during cycle #57

The bolted wedge design connector (AMP Part Number 81228-1), is a wedge pressure system comprised of a bronze body and wedge, with a copper alloy 'nest' and bronze shear head bolt. After the conductors have been inserted into the body, and the nest inserted between them, a tapered wedge is driven into the body, causing the body to spring open. The conductors are held together by a constant compressive force of the elastic body, trying to recover to its original shape. The connection is accomplished with a standard socket wrench (ratchet). Once the designed torque is reached on the shear head bolt, the bolt breaks away leaving the connection intact. **FIGURES 3 & 4** are photographs of AMP Part Number 81228-1, connectors #1 & #2 taken during the 100 cycle, current cycle test.



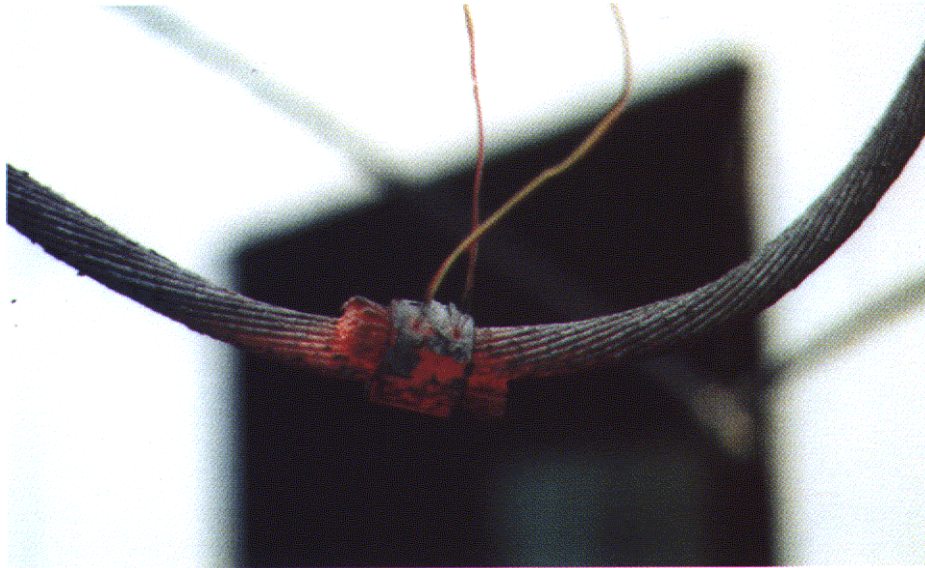


**FIGURE 3**  
AMP Bolted wedge connector #1  
Photograph taken during cycle #5

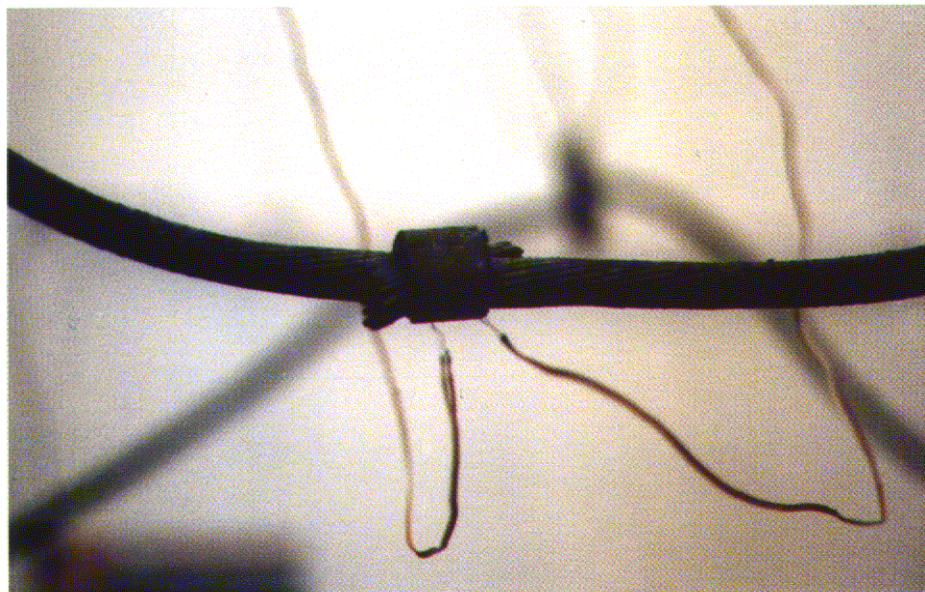


**FIGURE 4**  
AMP Bolted wedge connector #2  
Photograph taken during cycle #4  
Page (6)

The die compression type tap connectors, (Burndy Part Number YGHC29C29) are designed to accommodate two continuous parallel cables in the connector's conductor grooves. The connector is "C" shaped and requires a hydraulic compression tool with a U997 die to install. **FIGURES 5 & 6** are photographs of the die compression type tap connectors #1 & #2 taken during the 100 cycle, current cycle test.

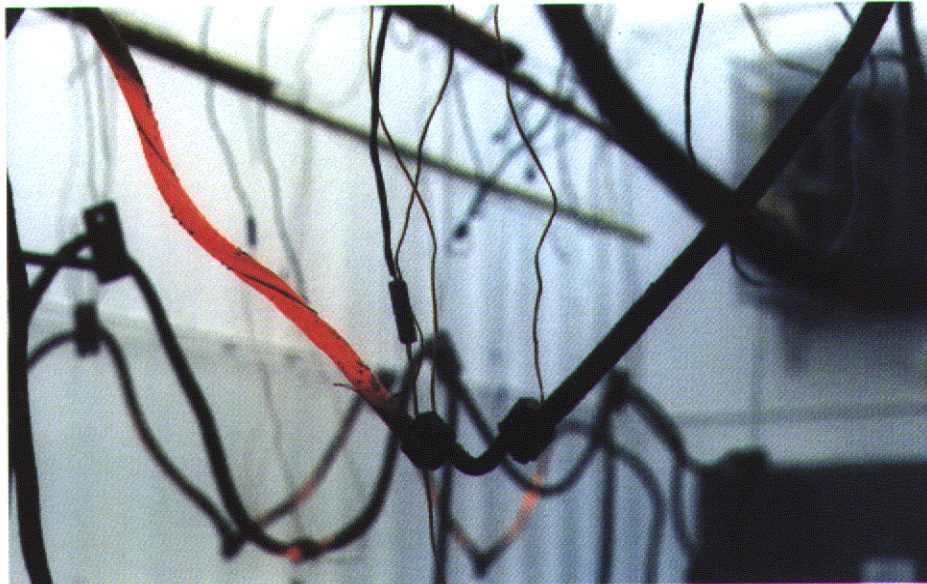


**FIGURE 5**  
Burndy YGHC29C29 die compression tap connector #1  
Photograph taken during cycle #10

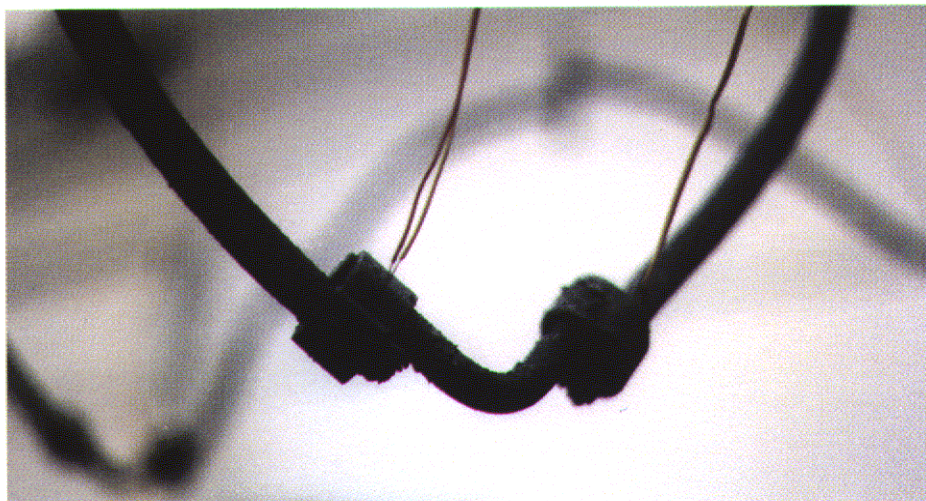


**FIGURE 6**  
Burndy YGHC29C29 die compression tap connector #2  
Photograph taken during cycle #10

The die compression type, cross connectors, (Burndy Part Number YGL29C29) are designed to make a 90° turn in the ground grid. Similar to the tap connector, the cross connector requires a hydraulic compression tool and a U997 die to install. The connector incorporates two 'C' elements with a 1/2 inch diameter copper rod bent to 90 degrees. When the conductors are inserted and the compression is made, the connector crimps both the conductor and copper rod making a rigid connection. Before crimping, both connector elements can be rotated on the copper rod to any desired position. **FIGURES 7 & 8** are photographs of the die compression type cross connectors #1 & #2 taken during the 100 cycle, current cycle test.

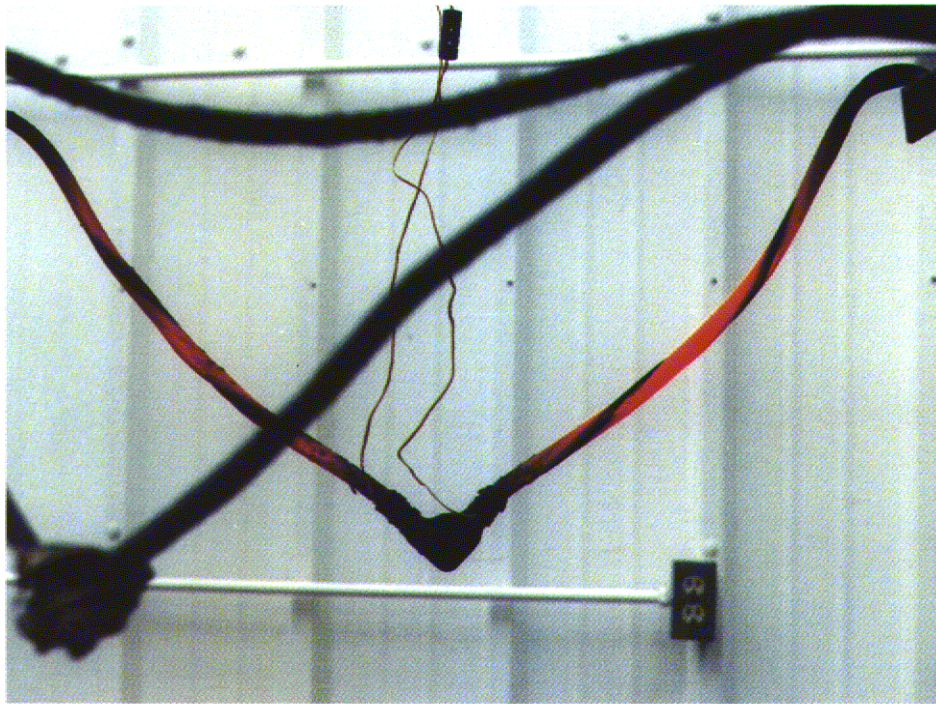


**FIGURE 7**  
Burndy YGL29C29 Die compression type cross connector #1  
Photograph taken during cycle #8



**FIGURE 8**  
Burndy YGL29C29 Die compression type cross connector #2  
Photograph taken during cycle #29

Another design of the die compression type cross connector tested was (Thomas & Betts Part Number GG40250-40250). This design connector is a one piece construction, also designed for making a 90 degree turn in the ground grid. The connector is designed for cable to cable or cable to rod installation. The connection requires a hydraulic compression tool with a 71H compression die. **FIGURE 9** is a photograph of Thomas & Betts die compression type cross connector #1 taken during the 100 cycle, current cycle test. Photograph of Thomas and Betts connector #2 is not available.



**FIGURE 9**  
T & B GG40250-40250 Die compression type cross connector #1  
Photograph taken during cycle #15

## TEST PROGRAM

### RESISTANCE

The thermal and electrical evaluation required one current cycle loop. Two connectors of each design, for each manufacturer, were tested. The complete loop contained ten connectors and a control conductor. The loop was prepared in accordance with IEEE Std. 837-1989. ILLUSTRATION 1 is a sketch of the loop as prepared and tested.

After placing the loop in the current cycle test fixture, type K thermocouples and permanent resistance leads were attached. Prior to energizing the loop with current, an initial voltage drop (resistance) reading was taken on each connector. The initial voltage drop reading is not used in the evaluation of the connector's performance; however, the reading was recorded as a base line for overall change. TABLE 1 contains the initial connector resistance values taken from voltage drop readings prior to energizing.

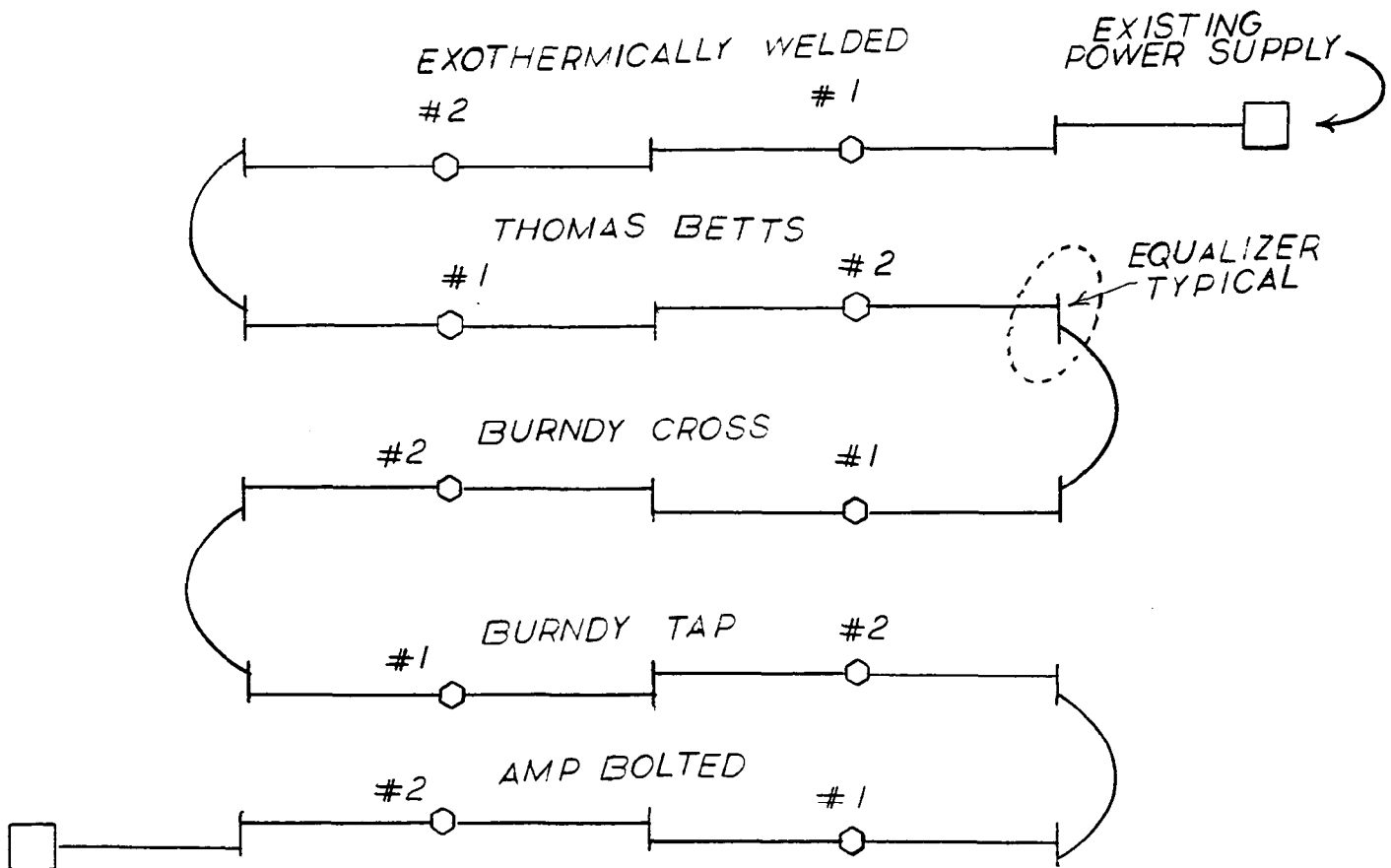


ILLUSTRATION 1

**TABLE 1**

<b>CONNECTOR RESISTANCE (IN MICROOHMS)*</b>	
Corrected to 20° Celsius	Total Connector Resistance Less Conductor
1) Cadweld® part number TAC2V2V welded connector #1	9
2) Cadweld® part number TAC2V2V welded connector #2	27
3) T & B part number GG40250 - 40250 cross connector #1	24
4) T & B part number GG40250 - 40250 cross connector #2	24
5) Burndy part number YCL29C29 cross connector #1	32
6) Burndy part number YGL29C29 cross connector #2	35
7) Burndy part number YGHC29C29 tap connector #1	146
8) Burndy part number YGHC29C29 tap connector #2	178
9) AMP part number 81228-1 bolted wedge connector #1	22
10) AMP part number 81228-1 bolted wedge connector #2	29
11) 48 inch length of control conductor	170

\* Connector resistance is the reading between two equalizers minus the control conductor resistance (IEEE Std. 837-1989)

The test loop was then energized with sufficient current to achieve a temperature of 550° Celsius on the control conductor. During load cycle one, the control conductor attained the 550° Celsius target temperature with 1,600 amperes of current; however, the resistance of some of the connections had increased the overall loop resistance to a magnitude that the existing power supply would not maintain the desired temperature. Consequently, the loop had to be removed from the connector laboratory, and taken to another location in the lab, with a power supply that had the capability of maintaining the desired current. **NOTE:** By the end of cycle one, all of the connectors with the exception of the exothermically welded Cadweld® connectors, had exceeded the temperature of the control conductor and failed the temperature requirement of IEEE Std. 837.

Care was taken to not disturb any of the connections during movement. The loop was moved as an entire assembly and nothing was taken apart. Prior to moving, the test loop was allowed to return to ambient temperature and another voltage drop reading was recorded. When the loop was installed at the new location, another voltage drop reading was recorded to assure that no damage was done to any of the connections during movement. It was observed that some resistance change had occurred during movement. The worst case was for the bolted wedge type connectors. **TABLE 2** contains the 'before and after movement' connector resistance values taken from voltage drop measurements.

**TABLE 2**

<b>CONNECTOR RESISTANCE (IN MICROOHMS)</b>		
<b>Corrected to 20° Celsius</b>	<b>BEFORE</b>	<b>AFTER</b>
1) Cadweld® part number TAC2V2V welded connector #1	10	1
2) Cadweld® part number TAC2V2V welded connector #2	7	23
3) T & B part number GG40250-40250 cross connector #1	172	143
4) T & B part number GG40250-40250 cross connector #2	178	179
5) Burndy part number YGL29C29 cross connector #1	117	97
6) Burndy part number YGL29C29 cross connector #2	64	70
7) Burndy part number YGHC29C29 tap connector #1	143	170
8) Burndy part number YGHC29C29 tap connector #2	75	65
9) AMP part number 81228-1 bolted wedge connector #1	26	38
10) AMP part number 81228-1 bolted wedge connector #2	57	145
11) 48 inch length of control conductor	173	176

At this point, the test loop was connected to a larger power supply, and the test was continued for the remaining 99 cycles. **TABLE 3** contains the resistance values recorded every tenth cycle for the duration of the test.

**TABLE 3**

CONNECTOR RESISTANCE VALUES EVERY TENTH CYCLE (IN MICROOHMS) LESS 48 INCH LENGTH OF CONTROL CONDUCTOR (IEEE STD. 837-1989) Corrected to 20° Celsius										
	CYCLE									
	10	20	30	40	50	60	70	80	90	100
EXOTHERMICALLY WELDED CADWELD® #1	-6	55	0	9	14	25	27	26	25	29
EXOTHERMICALLY WELDED CADWELD® #2	22	28	24	39	50	112	***	***	***	***
THOMAS & BETTS PN GG40250-40250 CROSS CONNECTOR #1	145	***	***	***	***	***	***	***	***	***
THOMAS & BETTS PN GG40250-40250 CROSS CONNECTOR #2	180	***	***	***	***	***	***	***	***	***
BURNDY PN YGL29C29 CROSS CONNECTOR #1	212	***	***	***	***	***	***	***	***	***
BURNDY PN YGL29C29 CROSS CONNECTOR #2	65	68	131	***	***	***	***	***	***	***
BURNDY PN YGHC29C29 TAP CONNECTOR #1	182	***	***	***	***	***	***	***	***	***
BURNDY PN YGHC29C29 TAP CONNECTOR #2	112	***	***	***	***	***	***	***	***	***
AMP PN 81221-1 BOLTED WEDGE #1	***	***	***	***	***	***	***	***	***	***
AMP PN 81221-1 BOLTED WEDGE #2	***	***	***	***	***	***	***	***	***	***
CONTROL CONDUCTOR RESISTANCE	204	207	198	221	233	226	230	234	245	249

\*\*\* Denotes shunted connector



## TEMPERATURE

### ERICO® EXOTHERMICALLY WELDED CADWELD® CONNECTION PART NUMBER TAC2V2V

The ERICO® exothermically welded Cadweld® connection #1 completed the 100 cycle, current cycle test without failure. The maximum temperature recorded during the 100 cycle test was 498° Celsius. At the time of the reading, the control conductor temperature was 551° Celsius.

The ERICO® exothermically welded Cadweld® connection #2 exceeded the temperature of the control conductor at cycle 58. The temperature of the connection was 553° and 533° Celsius at thermocouple locations one and two respectively. The control conductor temperature at the time of the reading was 549° Celsius. As stated in the summary, a 'hot spot' developed on the conductor approximately eight inches away from the connection due to a loss of cross sectional area of the conductor. The connection was allowed to continue to run until the conductor fusing occurred and burned in half at the 'hot spot' during cycle 64. The connector was shunted, and the test was allowed to continue. The shunts used in this test were 48 inch lengths of like conductor used in the test loop. The 48 inch length of shunt conductor was gas welded (brazed) into existing holes that were pre-drilled into the equalizers prior to starting the test.

### AMP BOLTED WEDGE CONNECTORS PART NUMBER 81228-1

During the first six cycles, the bolted wedge connectors began to increase significantly in temperature. The connectors began to glow bright orange within ten minutes into cycle three and arc periodically. By the conclusion of cycle four, bolted wedge connector #2, had reached a temperature of 894° Celsius and began to melt. At this point the connector ceased to perform, and current could no longer be passed through the connection. The connector was shunted with a 48 inch length of the same conductor used to assemble the loop, and the test was continued.

At cycle six, the remaining bolted wedge connector #1, reached a temperature of 960° Celsius. At this point the conductor melted inside the connector and separated. Again, the connection was shunted with a 48 inch length of conductor and the test was continued.

**BURNDY DIE COMPRESSION CROSS CONNECTOR**  
**PART NUMBER YGL29C29**

At cycle 14, the conductor used in the assembly of Burndy's Part Number YGL29C29, cross connector #1, burned in half approximately five inches from the connector. The connector temperature had exceeded the temperature of the control conductor at both thermocouple locations (642 and 619 degrees Celsius). The conductor developed a hot spot, due to the loss of cross sectional area during the thermal cycling, and eventually burned and separated.

At cycle 18, the same failure mode occurred for cross connector #2. The conductor burned and separated approximately nine inches from the crimped connection. The connector temperature at the time of the conductor failure was 622 and 601 degrees Celsius.

**BURNDY DIE COMPRESSION TAP CONNECTOR**  
**PART NUMBER YGHC29C29**

At cycle 17, the conductor used to join Burndy's tap connector #1, burned in half at the connection. At the time of conductor failure, the connector temperature, at both thermocouple locations was 646 and 658 degrees Celsius; however, during previous cycles earlier in the test, the connector temperature reached a temperature of 719 and 734 degrees Celsius.

At cycle 34, the conductor used to join Burndy's tap connector #2, burned in half at the connection. The same failure mode is suspected in connection #2 as in connection #1 due to similarities. At the time of the failure, the connection had reached a temperature of 625 and 608 degrees Celsius. During previous cycles, the connection had reached temperatures of 716 and 709 degrees Celsius.

**THOMAS & BETTS DIE COMPRESSION CROSS CONNECTOR**  
**PART NUMBER GG40250-40250**

At cycle 20, the conductor used to join Thomas & Betts cross connector #2, burned in half approximately four inches from the connector. At the time of conductor failure the connector temperature at both thermocouple locations was 644 and 596 degrees Celsius. The maximum temperature attained on the connector was 674 degrees Celsius during cycle 17.

At cycle 21, the conductor used to join Thomas & Betts cross connector #1, burned in half at the connector. At the time of the failure, the connector temperature was 705 and 708 degrees Celsius.

**TABLE 4** shows the maximum temperatures, recorded at the end of each listed cycle, for all connectors tested. **BOLD TYPE** indicates that the connection temperature is operating at a higher temperature than the control conductor temperature.

#### **TEST EQUIPMENT**

To conduct the 100 cycle, current cycle test, the following equipment was used.

- Current cycle test power supply
- Fluke data acquisition unit, Model #2280B
- Biddle low resistance ohm meter, Model DLRO, Catalog #PN 15572-1

**TABLE 4**

<b>TEMPERATURE DEGREES CELSIUS FOR LAST READING OF EACH RECORDED CYCLE</b>						
<b>CYCLE NUMBER</b>	<b>CONTROL TEMP.</b>	<b>EXOTHERMIC CADWELD #1 TC #1 TC #2</b>	<b>EXOTHERMIC CADWELD #2 TC #1 TC #2</b>	<b>THOMAS &amp; BETTS CROSS CONNECTOR #1 TC #1 TC #2</b>	<b>THOMAS &amp; BETTS CROSS CONNECTOR #2 TC #1 TC #2</b>	
1	544	472 477	465 462	577 581	581 575	
2	550	485 496	469 463	608 602	607 597	
3	551	479 498	466 460	598 592	594 584	
4	552	475 483	464 451	592 589	595 589	
5	552	471 479	463 448	589 588	596 587	
6	553	469 475	459 452	592 596	607 593	
7	551	465 471	451 443	607 604	608 591	
8	551	464 470	454 453	601 603	618 596	
9	551	465 469	458 473	606 560	628 583	
10	549	463 469	466 477	611 581	601 595	
11	550	466 471	462 455	614 589	597 591	
12	552	465 469	470 458	599 586	603 598	
13	550	465 470	470 477	615 598	615 598	
14	550	465 470	473 477	602 569	630 599	
15	549	464 469	471 473	617 600	625 598	
16	548	464 469	472 472	620 622	634 597	
17	554	467 472	476 477	612 626	674 612	
18	550	468 474	487 481	578 606	660 616	
19	549	470 474	488 482	620 630	644 596	
20	547	469 472	488 482	705 708	SHUNT	
21	550	469 473	487 482	SHUNT		
22	550	467 471	486 481			
23	551	466 469	487 481			
24	550	466 469	485 479			
25	551	467 471	487 481			

**TABLE 4**

<b>TEMPERATURE DEGREES CELSIUS FOR LAST READING OF EACH RECORDED CYCLE</b>					
<b>CYCLE NUMBER</b>	<b>CONTROL TEMP.</b>	<b>EXOTHERMIC CADWELD #1 TC #1 TC #2</b>	<b>EXOTHERMIC CADWELD #2 TC #1 TC #2</b>	<b>THOMAS &amp; BETTS CROSS CONNECTOR #1 TC #1 TC #2</b>	<b>THOMAS &amp; BETTS CROSS CONNECTOR #2 TC #1 TC #2</b>
26	549	466 470	495 481	SHUNT	SHUNT
27	552	465 468	487 481		
28	550	468 471	490 484		
29	552	467 469	489 483		
30	552	467 470	489 484		
31	549	468 471	488 482		
32	551	468 471	489 483		
33	548	470 473	485 478		
34	551	472 475	494 488		
35	547	469 472	492 486		
36	552	473 467	500 493		
37	550	471 474	499 491		
38	550	470 473	498 490		
39	544	466 468	494 487		
40	549	472 475	497 490		
41	549	472 475	498 490		
42	544	474 477	504 494		
43	547	474 477	501 492		
44	551	477 481	510 501		
45	548	476 479	507 498		
46	549	469 473	505 495		
47	551	470 472	504 494		
48	549	475 478	507 497		
49	549	478 481	513 503		
50	547	478 480	505 494		

**TABLE 4**

<b>TEMPERATURE DEGREES CELSIUS FOR LAST READING OF EACH RECORDED CYCLE</b>					
<b>CYCLE NUMBER</b>	<b>CONTROL TEMP.</b>	<b>EXOTHERMIC CADWELD #1 TC #1 TC #2</b>	<b>EXOTHERMIC CADWELD #2 TC #1 TC #2</b>	<b>THOMAS &amp; BETTS CROSS CONNECTOR #1 TC #1 TC #2</b>	<b>THOMAS &amp; BETTS CROSS CONNECTOR #2 TC #1 TC #2</b>
51	546	476 479	510 500	SHUNT	SHUNT
52	551	478 481	518 505		
53	552	480 483	531 517		
54	551	480 483	533 517		
55	552	479 482	537 520		
56	553	478 481	540 523		
57	540	470 473	539 521		
58	549	474 477	553 533		
59	551	477 481	561 541		
60	549	474 477	559 538		
61	549	472 475	556 535		
62	550	473 476	562 541		
63	551	476 478	573 551		
64	550	474 477	591 565		
65	549	474 477	SHUNT		
66	546	470 473			
67	552	475 478			
68	551	473 476			
69	547	472 476			
70	554	477 481			
71	548	473 477			
72	554	478 482			
73	547	459 463			
74	544	454 459			
75	552	458 463			

**TABLE 4**

<b>TEMPERATURE DEGREES CELSIUS FOR LAST READING OF EACH RECORDED CYCLE</b>					
<b>CYCLE NUMBER</b>	<b>CONTROL TEMP.</b>	<b>EXOTHERMIC CADWELD #1 TC #1 TC #2</b>	<b>EXOTHERMIC CADWELD #2 TC #1 TC #2</b>	<b>THOMAS &amp; BETTS CROSS CONNECTOR #1 TC #1 TC #2</b>	<b>THOMAS &amp; BETTS CROSS CONNECTOR #2 TC #1 TC #2</b>
76	552	460 464	SHUNT	SHUNT	SHUNT
77	550	456 460			
78	552	459 462			
79	554	460 464			
80	549	454 458			
81	555	462 466			
82	550	457 461			
83	556	462 466			
84	550	460 464			
85	550	459 463			
86	544	454 459			
87	549	456 459			
88	554	458 460			
89	551	457 462			
90	549	455 459			
91	547	450 455			
92	554	449 452			
93	548	452 456			
94	552	458 463			
95	550	455 460			
96	555	462 466			
97	545	455 459			
98	551	461 464			
99	550	459 463			
100	550	461 465			

**TABLE 4**

<b>TEMPERATURE DEGREES CELSIUS FOR LAST READING OF EACH RECORDED CYCLE</b>									
<b>CYCLE NUMBER</b>	<b>CONTROL TEMP.</b>	<b>BURNDY CROSS CONNECTOR #1</b>		<b>BURNDY CROSS CONNECTOR #2</b>		<b>BURNDY TAP CONNECTOR #1</b>		<b>BURNDY TAP CONNECTOR #2</b>	
		<b>TC #1</b>	<b>TC #2</b>	<b>TC #1</b>	<b>TC #2</b>	<b>TC #1</b>	<b>TC #2</b>	<b>TC #1</b>	<b>TC #2</b>
1	544	618	606	618	619	613	613	601	590
2	550	625	620	643	634	678	691	663	636
3	551	624	619	637	626	691	704	667	644
4	552	628	633	652	641	697	713	654	676
5	552	628	633	654	646	712	726	671	667
6	553	640	630	650	643	714	726	702	692
7	551	649	628	651	644	719	734	716	709
8	551	663	625	660	673	697	710	668	660
9	551	648	623	640	674	698	711	686	680
10	549	652	619	638	667	698	710	681	675
11	550	644	610	644	669	691	703	679	699
12	552	643	618	645	668	609	622	663	653
13	550	642	619	637	635	628	640	647	623
14	550	SHUNT		638	636	630	642	657	633
15	549			618	626	633	645	663	642
16	548			620	621	646	658	669	648
17	554			622	601	SHUNT		702	679
18	550			SHUNT				541	527
19	549							567	548
20	547							562	543
21	550							565	535
22	550							559	528
23	551							563	535
24	550							562	534
25	551							567	539



**TABLE 4**

<b>TEMPERATURE DEGREES CELSIUS FOR LAST READING OF EACH RECORDED CYCLE</b>					
<b>CYCLE NUMBER</b>	<b>CONTROL TEMP.</b>	<b>BURNDY CROSS CONNECTOR #1 TC #1 TC #2</b>	<b>BURNDY CROSS CONNECTOR #2 TC #1 TC #2</b>	<b>BURNDY TAP CONNECTOR #1 TC #1 TC #2</b>	<b>BURNDY TAP CONNECTOR #2 TC #1 TC #2</b>
26	549	SHUNT	SHUNT	SHUNT	568 541
27	552				576 548
28	550				577 545
29	552				579 545
30	552				587 556
31	549				593 576
32	551				607 593
33	548				625 608
34					SHUNT

**TABLE 4**

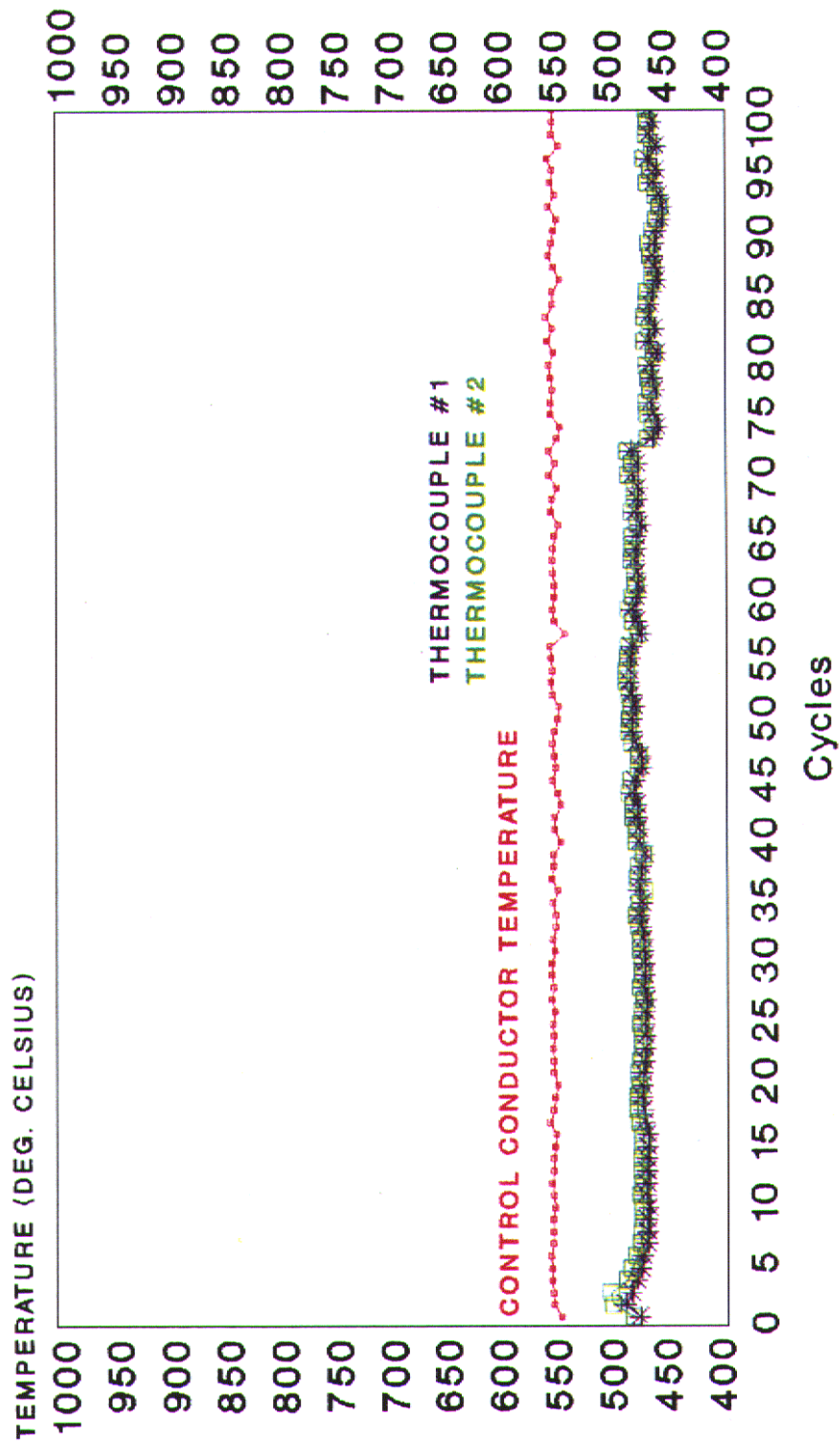
TEMPERATURE DEGREES CELSIUS FOR LAST READING OF EACH RECORDED CYCLE							
CYCLE NUMBER	CONTROL TEMP.	AMP BOLT WEDGE CONNECTOR #1		AMP BOLT WEDGE CONNECTOR #2			
		TC #1	TC #2	TC #1	TC #2		
1	544	612	619	778	658		
2	550	628	650	850	676		
3	551	691	809	886	691		
4	552	620	853	863	894		
5	552	624	851	SHUNT			
6	549	656	960				
		SHUNT					

## **APPENDIX 1**

# COMPARATIVE GROUNDING CONNECTOR TEST

## CADWELD PART NUMBER TAC2V2V SAMPLE #1

### EXOTHERMICALLY WELDED



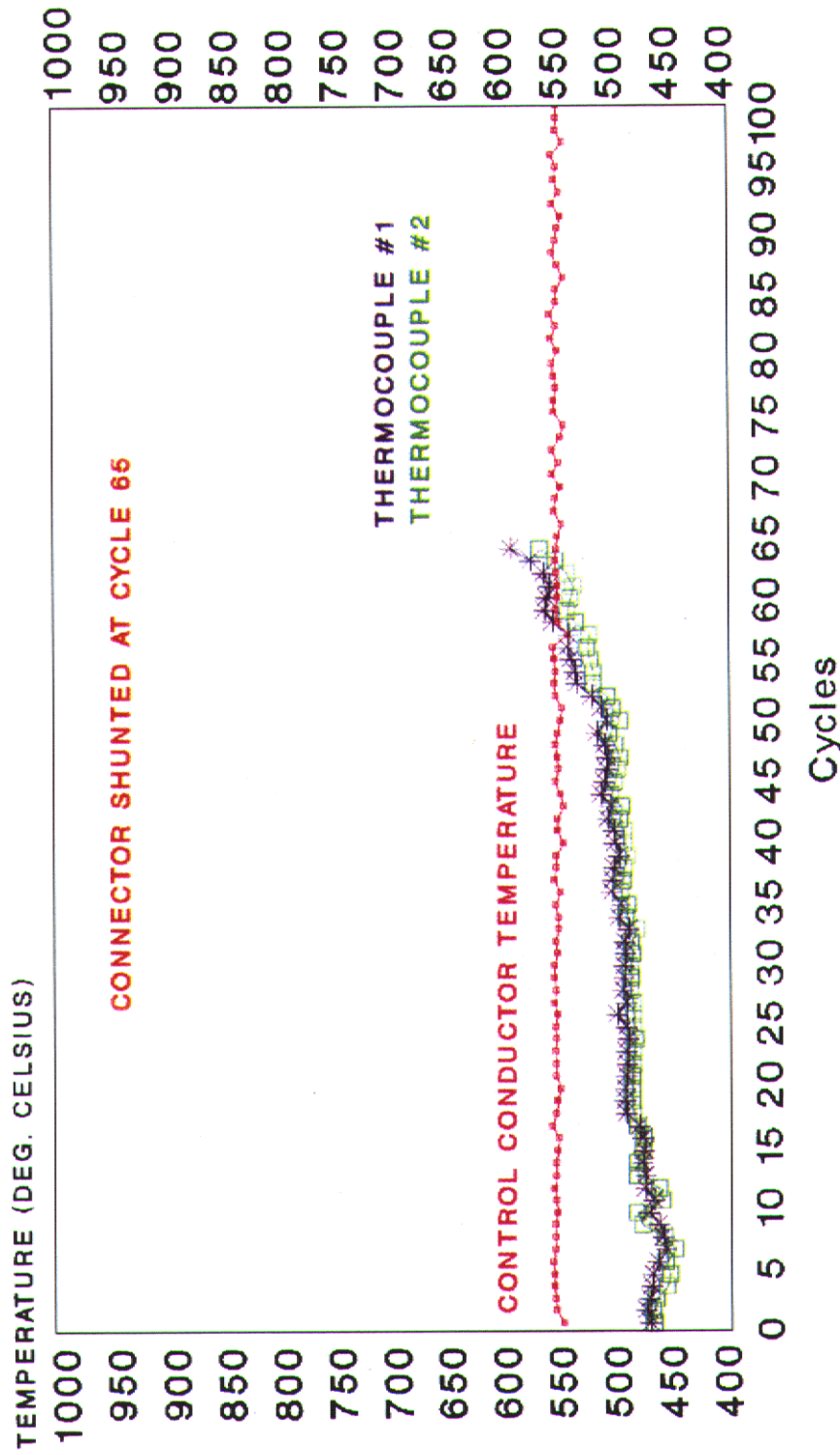
TESTED ON 250 KCMIL, 37 STRAND COPPER  
IEEE 837 THERMAL CYCLE TEST (MODIFIED)

TESTED AT GEORGIA POWER RESEARCH CENTER

# COMPARATIVE GROUNDING CONNECTOR TEST

## CADWELD PART NUMBER TAC2V2V SAMPLE #2

### EXOTHERMICALLY WELDED



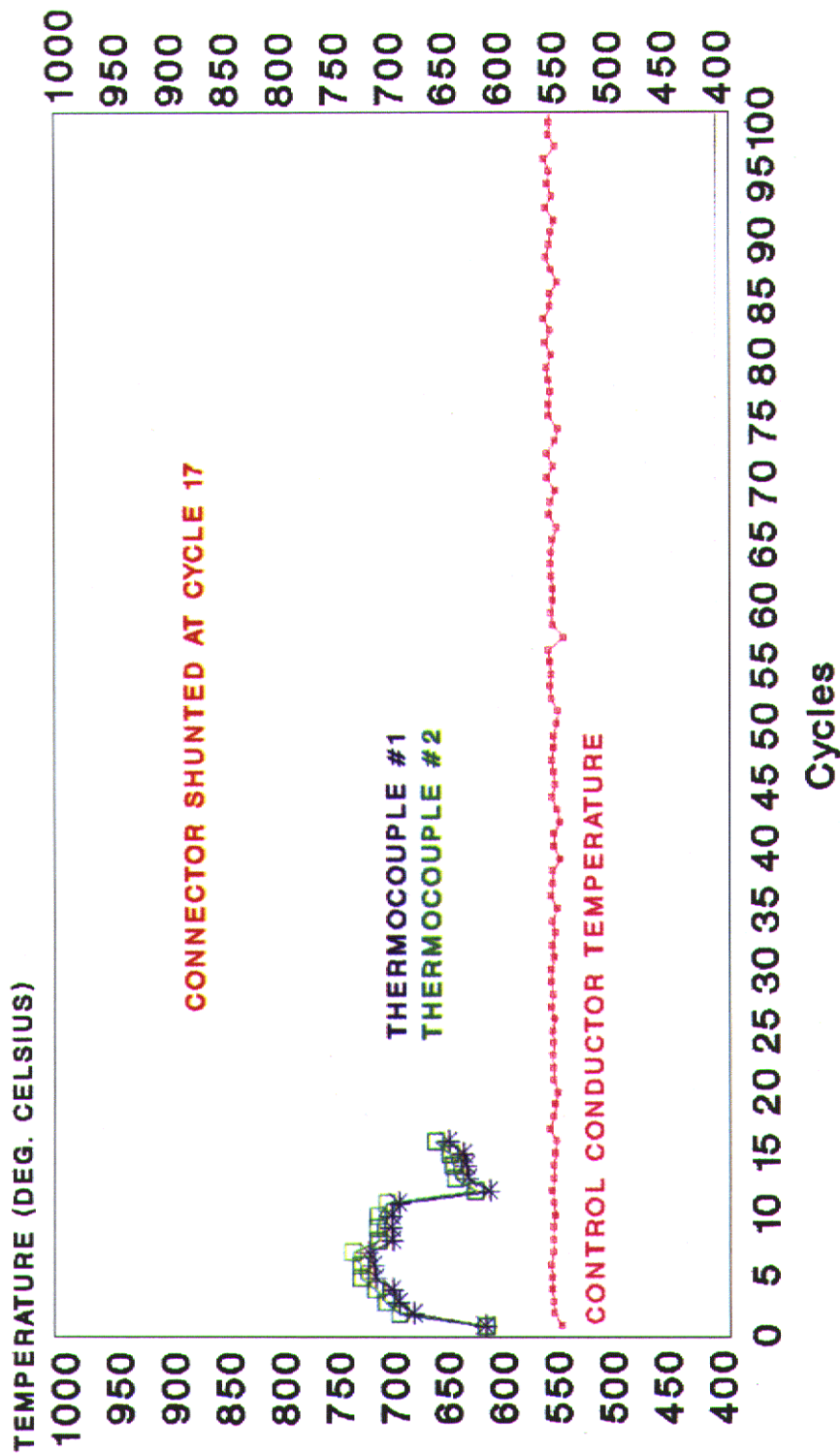
TESTED ON 250 KCMIL, 37 STRAND COPPER  
 IEEE 837 THERMAL CYCLE TEST (MODIFIED)

TESTED AT GEORGIA POWER RESEARCH CENTER

# COMPARATIVE GROUNDING CONNECTOR TEST

## BURNDY PART NUMBER YGHC29C29 SAMPLE #1

### TAP CONNECTOR



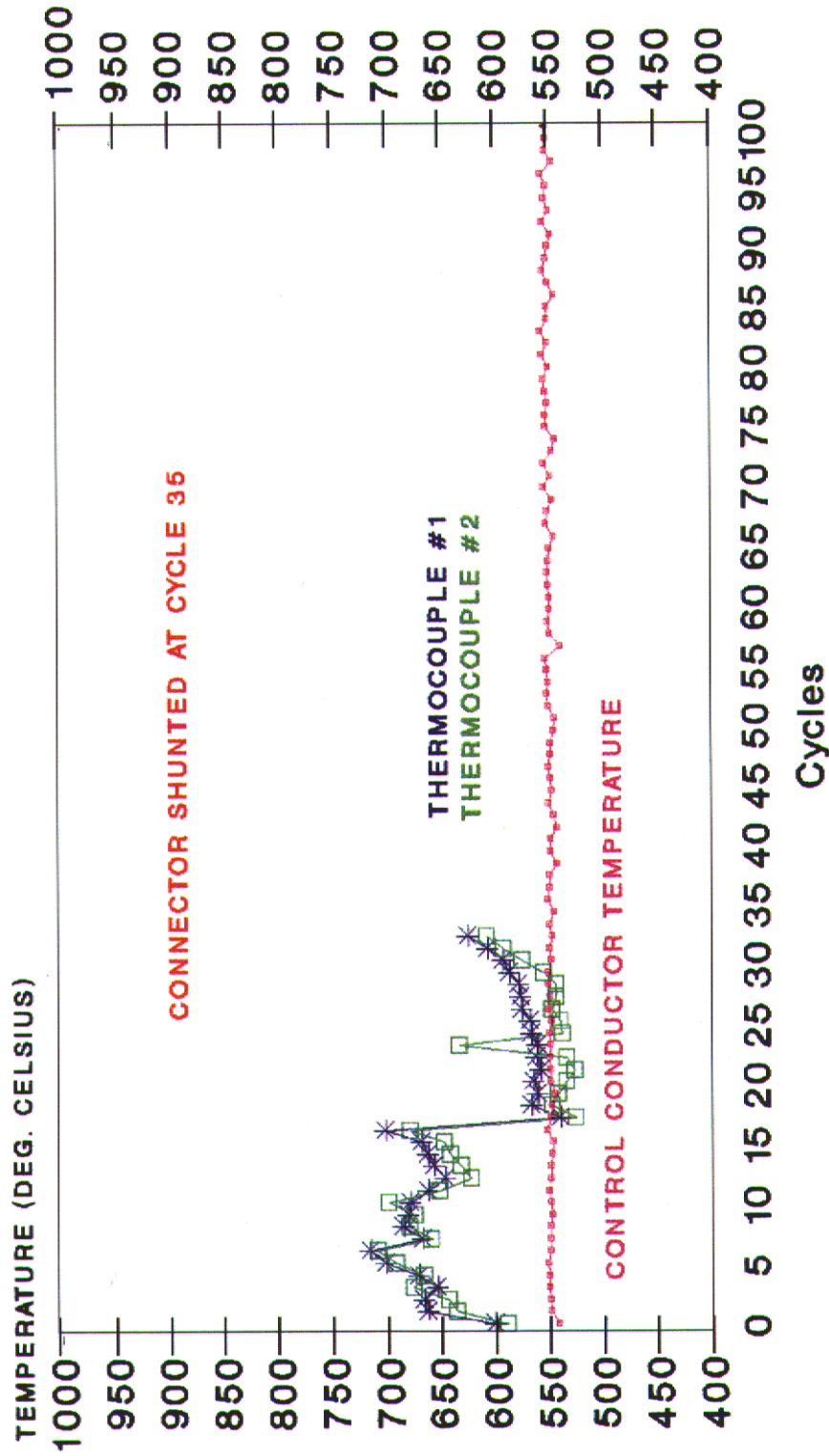
TESTED ON 250 KCMIL, 37 STRAND COPPER  
IEEE 837 THERMAL CYCLE TEST (MODIFIED)

TESTED AT GEORGIA POWER RESEARCH CENTER

# COMPARATIVE GROUNDING CONNECTOR TEST

## BURNDY PART NUMBER YGHC29C29 SAMPLE #2

### TAP CONNECTOR



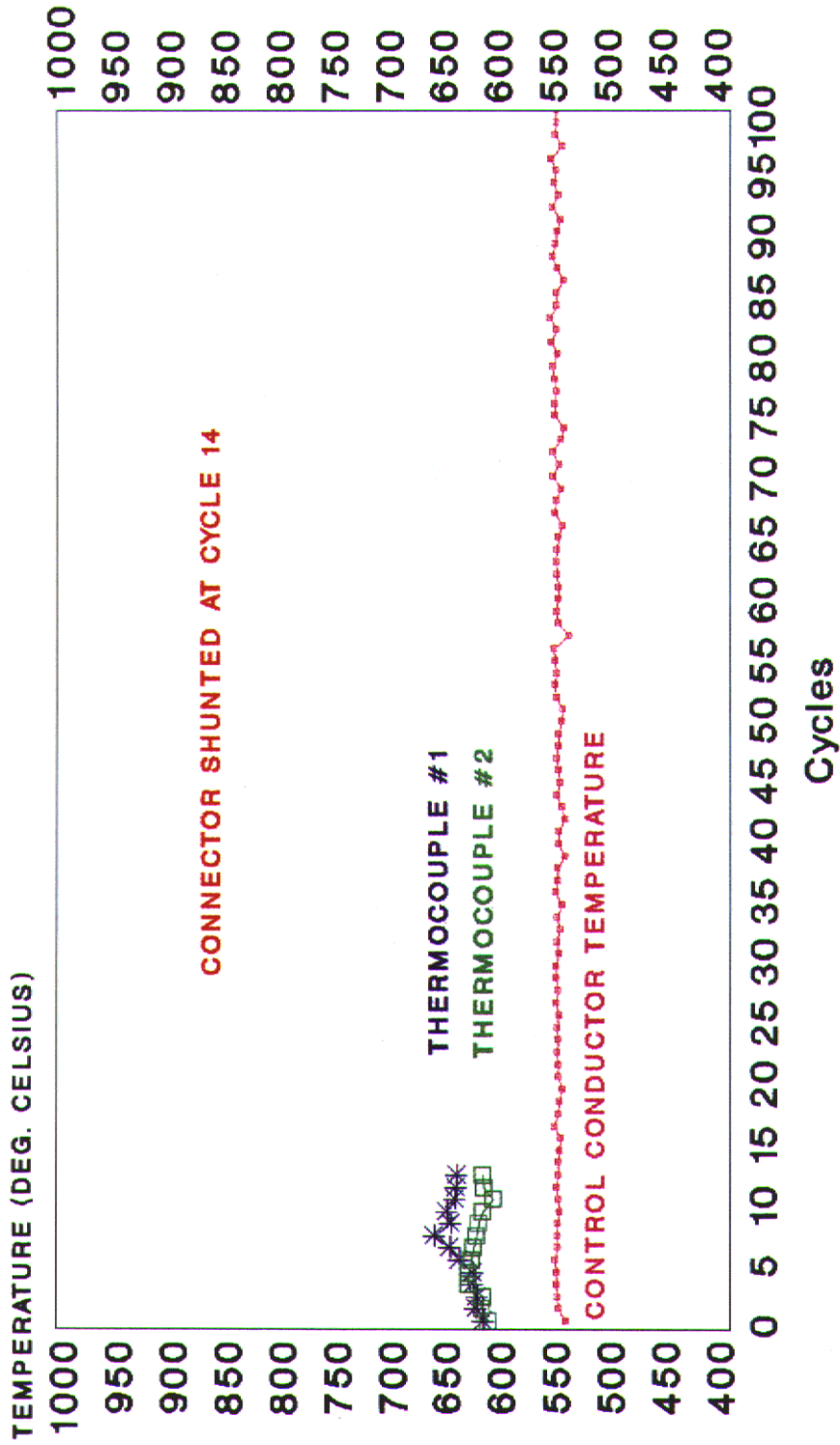
TESTED ON 250 KCMIL, 37 STRAND COPPER  
IEEE 837 THERMAL CYCLE TEST (MODIFIED)

TESTED AT GEORGIA POWER RESEARCH CENTER

# COMPARATIVE GROUNDING CONNECTOR TEST

## BURNDY PART NUMBER YGL29C29 SAMPLE #1

### CROSS CONNECTOR



TESTED ON 250 KCMIL, 37 STRAND COPPER  
IEEE 837 THERMAL CYCLE TEST (MODIFIED)

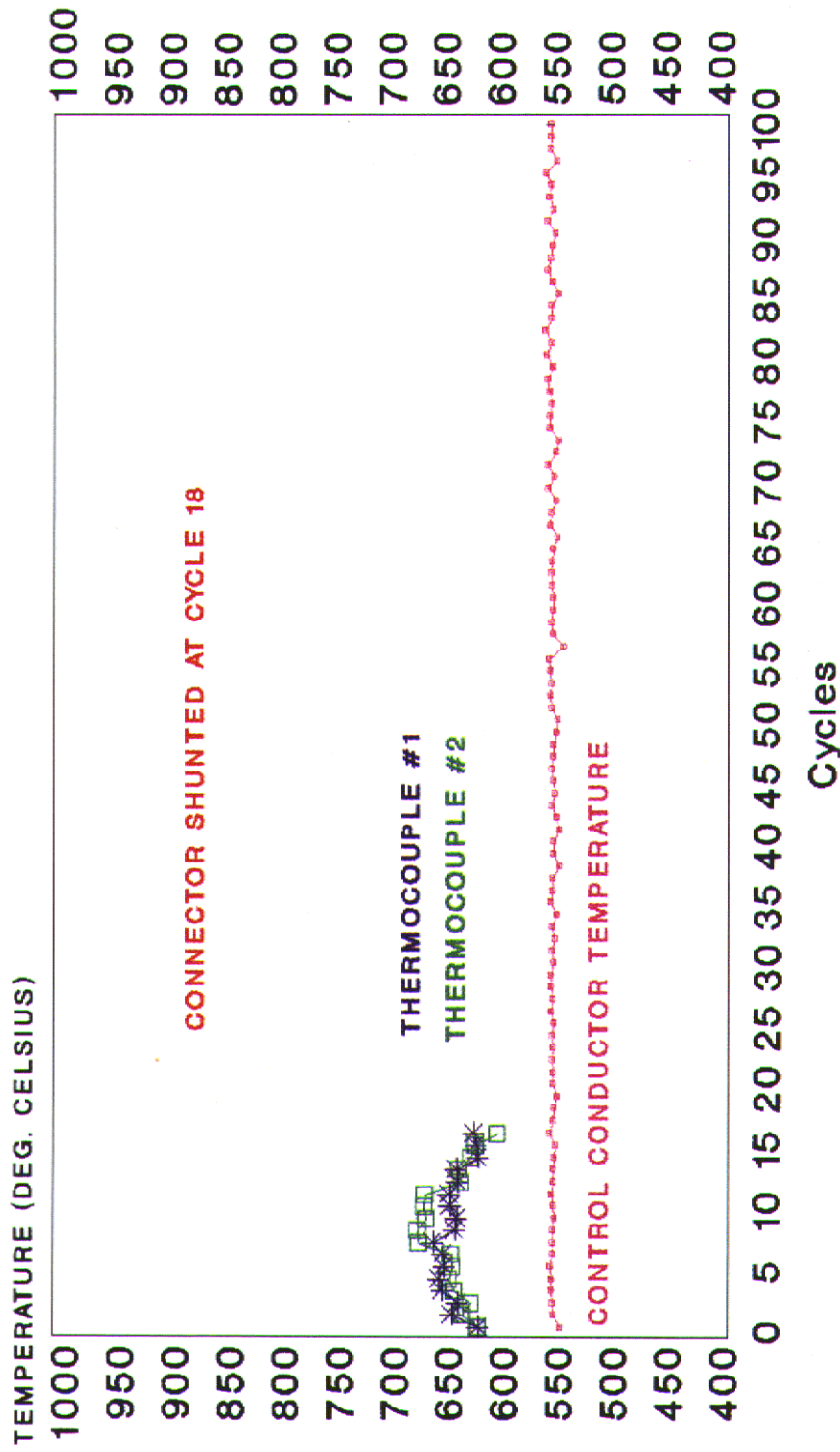
TESTED AT GEORGIA POWER RESEARCH CENTER



# COMPARATIVE GROUNDING CONNECTOR TEST

## BURNDY PART NUMBER YGL29C29 SAMPLE #2

### CROSS CONNECTOR



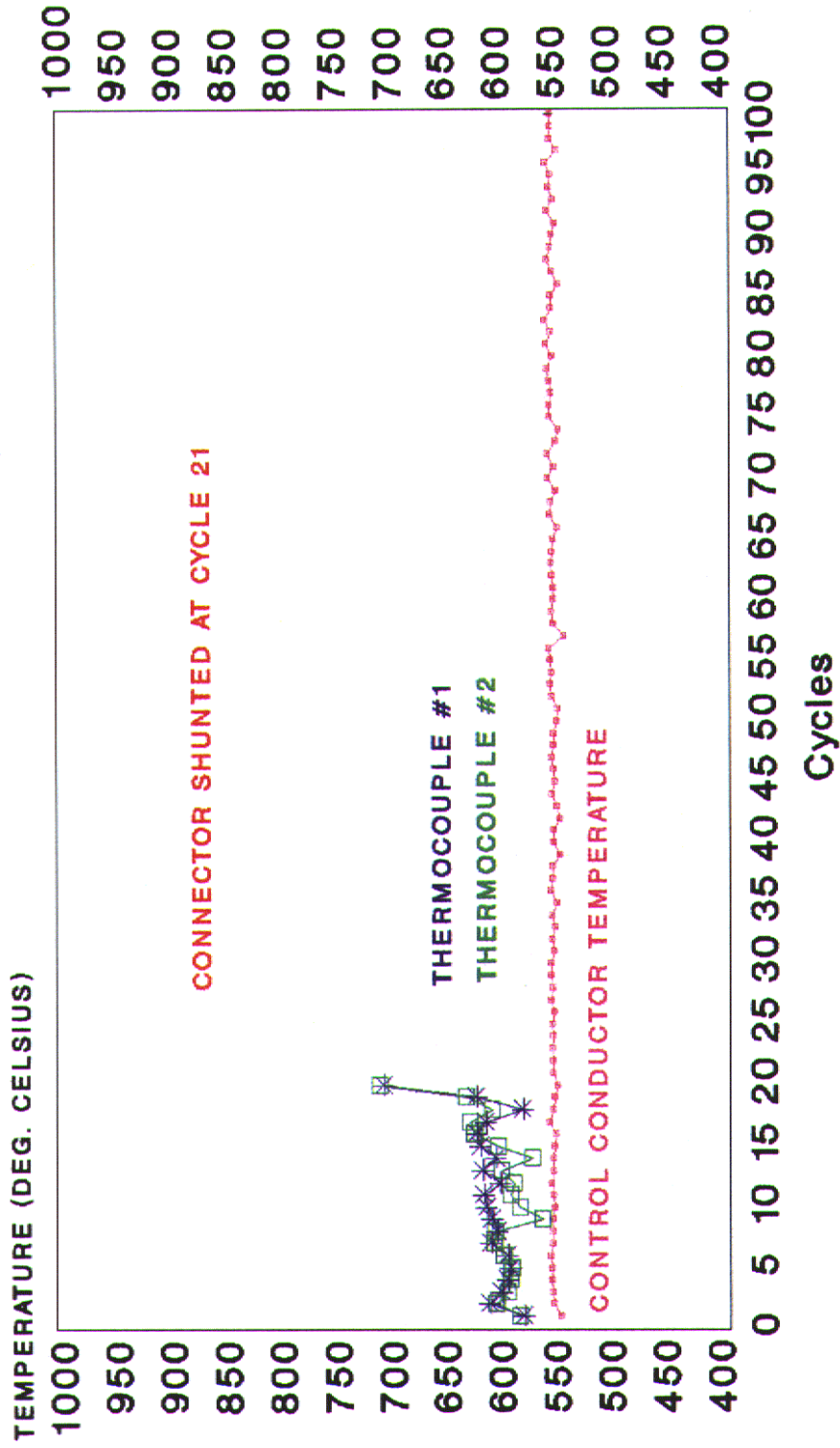
TESTED ON 250 KCMIL, 37 STRAND COPPER  
 IEEE 837 THERMAL CYCLE TEST (MODIFIED)

TESTED AT GEORGIA POWER RESEARCH CENTER

# COMPARATIVE GROUNDING CONNECTOR TEST

## T&B PART NUMBER GG40250-40250 SAMPLE #1

### CROSS CONNECTOR



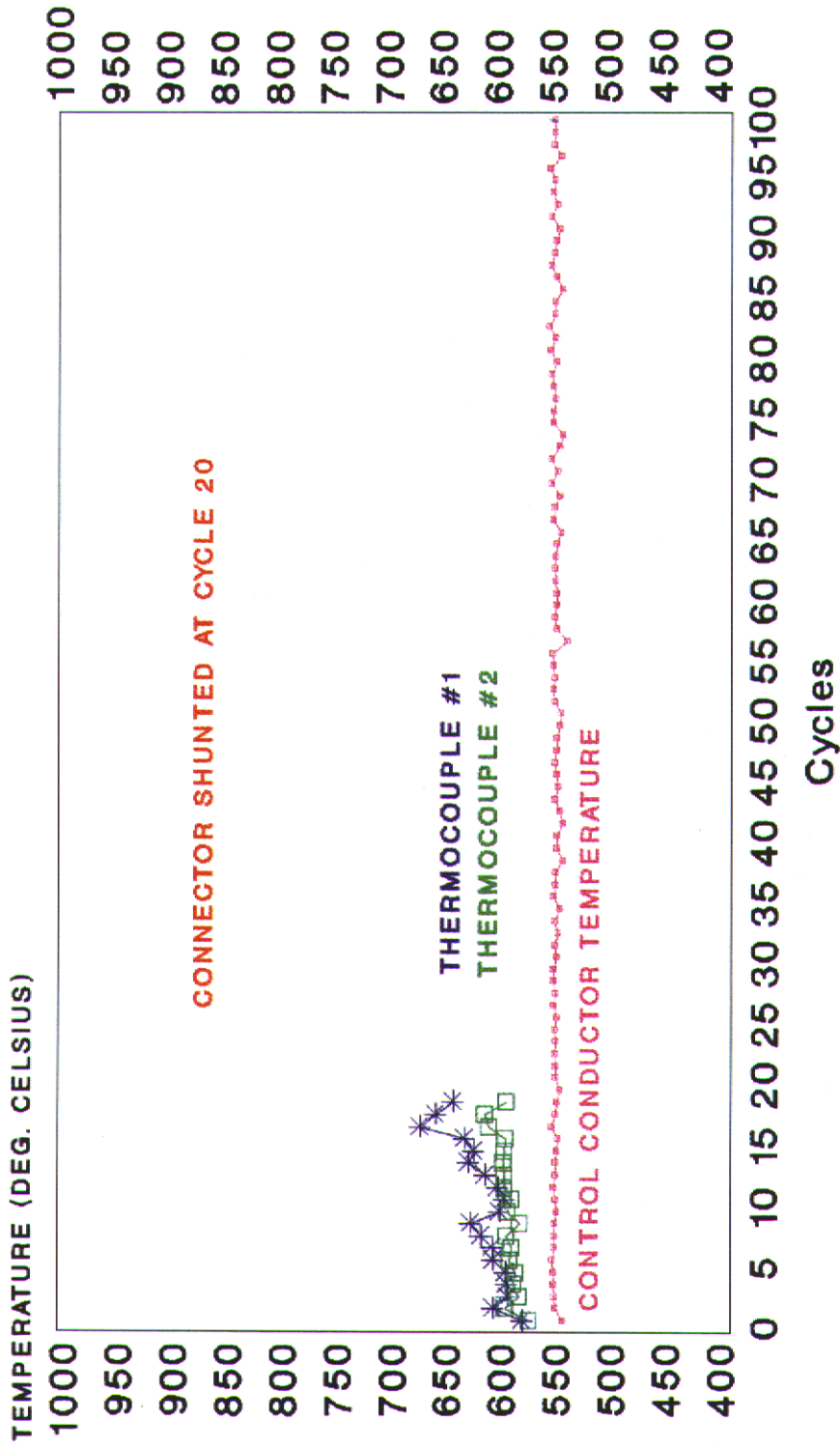
TESTED ON 250 KCMIL, 37 STRAND COPPER  
 IEEE 837 THERMAL CYCLE TEST (MODIFIED)

TESTED AT GEORGIA POWER RESEARCH CENTER

# COMPARATIVE GROUNDING CONNECTOR TEST

## T&B PART NUMBER GG40250-40250 SAMPLE #2

### CROSS CONNECTOR

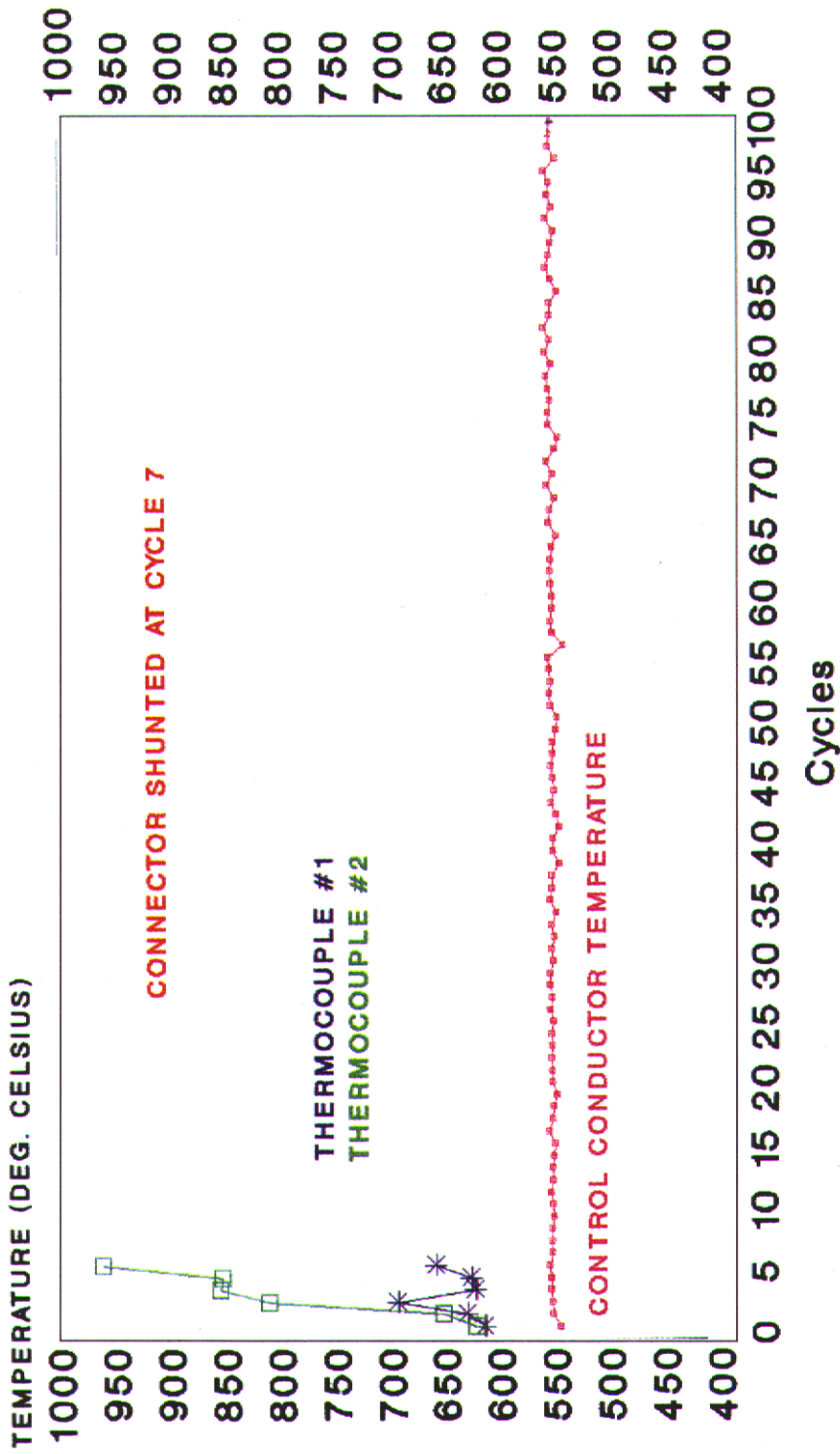


TESTED ON 250 KCMIL, 37 STRAND COPPER  
 IEEE 837 THERMAL CYCLE TEST (MODIFIED)  
 TESTED AT GEORGIA POWER RESEARCH CENTER

# COMPARATIVE GROUNDING CONNECTOR TEST

## AMP PART NUMBER 81228-1 SAMPLE #1

### BOLTED WEDGE CONNECTOR



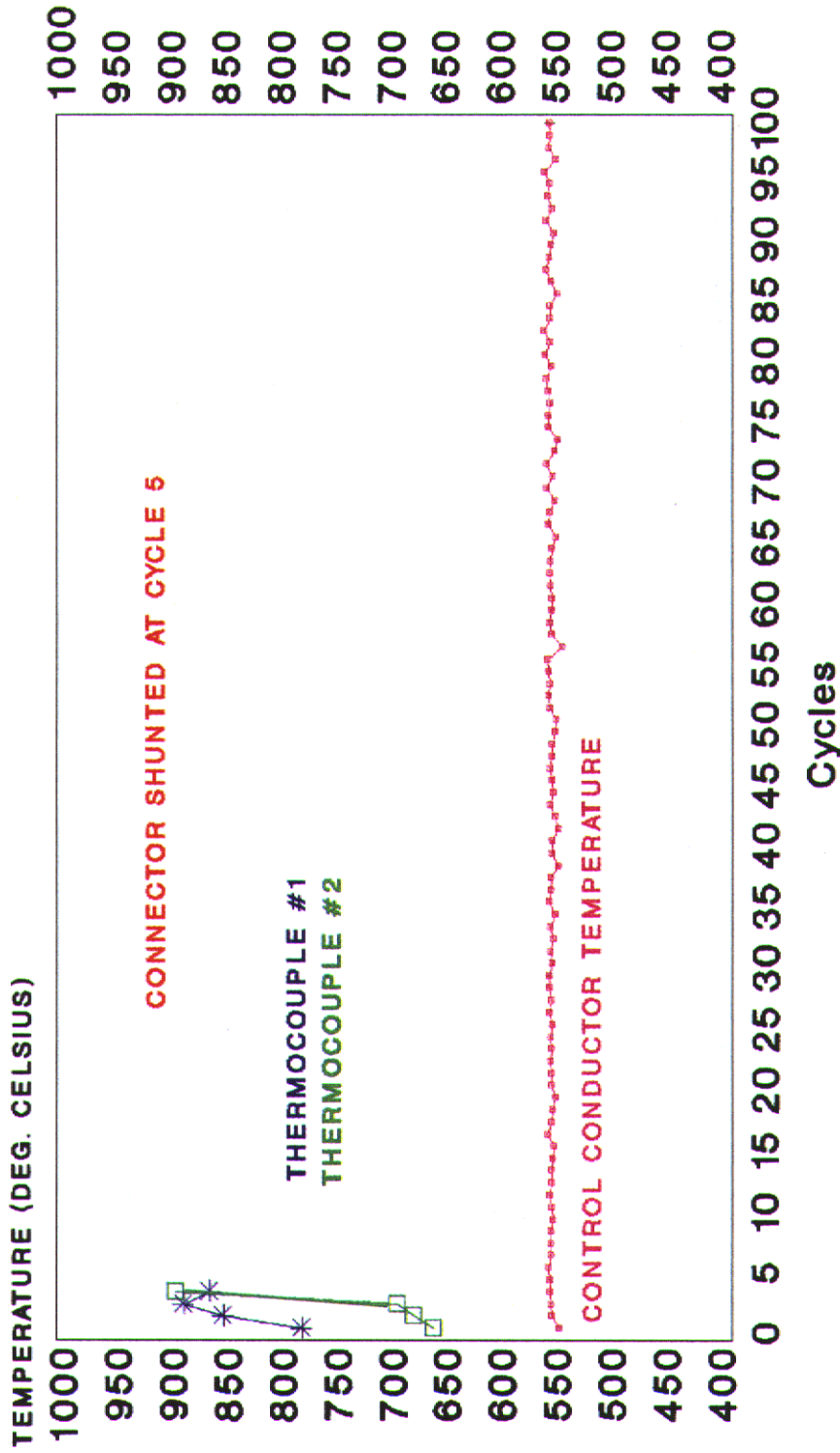
TESTED ON 250 KCMIL, 37 STRAND COPPER  
 IEEE 837 THERMAL CYCLE TEST (MODIFIED)

TESTED AT GEORGIA POWER RESEARCH CENTER

# COMPARATIVE GROUNDING CONNECTOR TEST

## AMP PART NUMBER 81228-1 SAMPLE #2

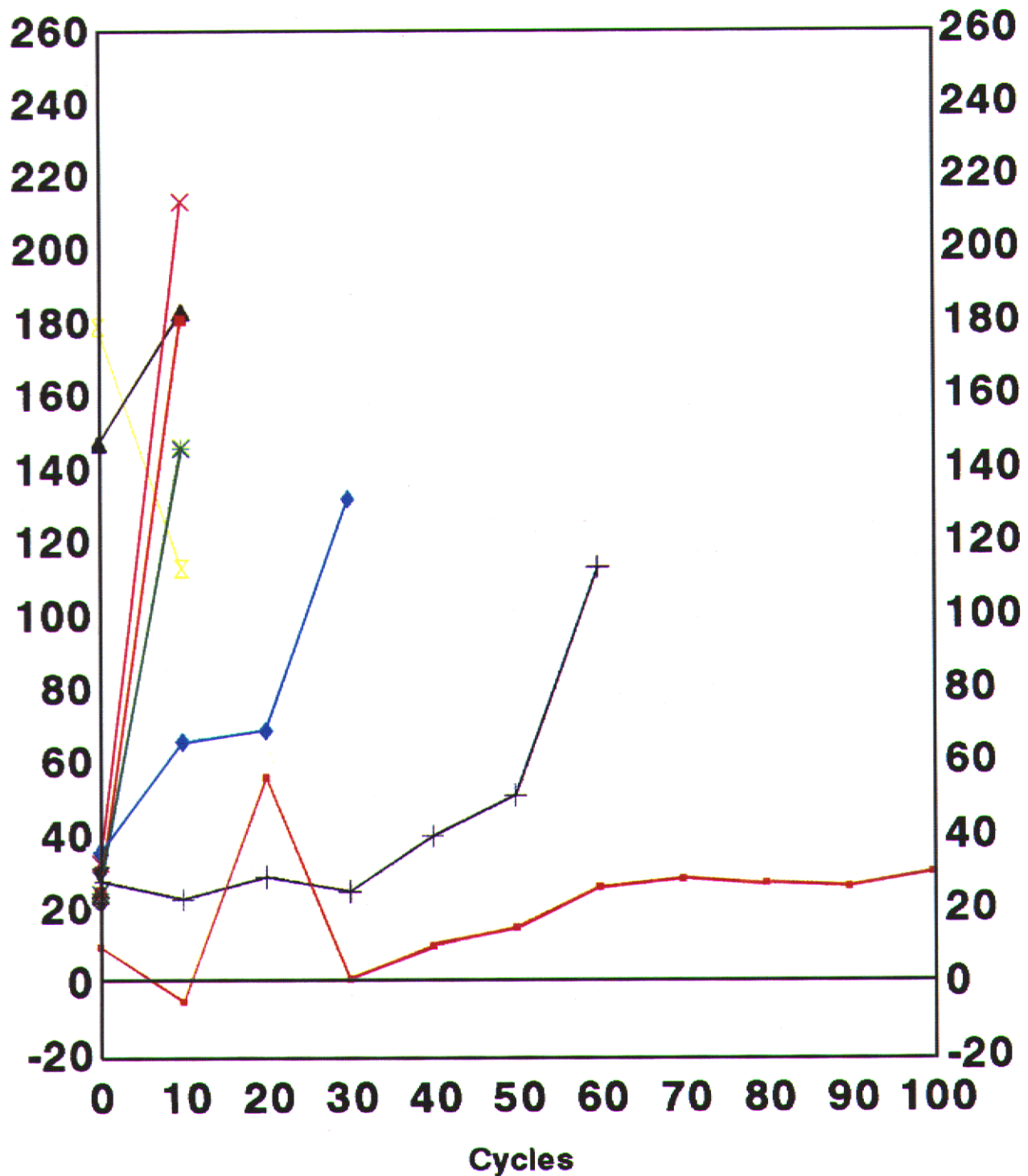
### BOLTED WEDGE CONNECTOR



TESTED ON 250 KCMIL, 37 STRAND COPPER  
IEEE 837 THERMAL CYCLE TEST (MODIFIED)

TESTED AT GEORGIA POWER RESEARCH CENTER

## COMPARATIVE GROUNDING CONNECTOR TEST RESISTANCE VALUES IN MICROOHMS



- CADWELD #1
  CADWELD #2
  T & B #1
  T & B #2
- BRN CROSS #1
  BRN CROSS #2
  BRN TAP #1
  BRN TAP #2
- AMP BOLT #1
  AMP BOLT #2

## **APPENDIX 2**

having an asymmetry, and the magnitude as stated above.

NOTE: Using this as a parameter to prove that a connection would survive the most severe forces encountered during a fault, the asymmetrical current value was selected for the test.

The maximum fusing current value of 100 000 A rms symmetrical was chosen because this is the highest value anticipated by utilities.

It is assumed that fault current will divide equally and flow in two directions when entering the ground grid.

**7.3.5 Number of Surges.** The test shall consist of three surges. Repeat each surge after the conductor has been allowed to cool to 100 °C or less.

**7.3.6 Resistance Measurements.** Resistance readings shall be recorded for each sample, in accordance with 8.8 initially, and after the three fault surges when samples have returned to ambient temperature.

## 8. Current-Temperature Cycling Test

**8.1 General.** This test is intended to assure the conformance to resistance criteria of connections subjected to temperature changes caused by fluctuating currents.

**8.2 Current-Temperature Cycling Test.** This test shall be the first test conducted in a series of sequential tests, as listed in Table 1.

**8.2.1 Conductor Combinations.** When joining different types or sizes of conductors, the selection of the conductor combinations and test current shall be that which results in the highest connector temperature while producing the conductor temperatures specified in Table 5.

*Example 1:* Connector for 3/4-1 in galvanized steel rod to #6-#2 copper wire. From Table 6, test currents are 3/4 in rod—274 A, 1 in rod—324 A, #6 wire—230 A, #4 wire—320 A, and #2 wire—440 A. Select a 1 in galvanized steel rod and #4 copper wire and use an initial test current of 320 A, which should achieve a 250 °C temperature on the galvanized steel rod.

*Example 2:* Connector for 1/2-5/8 in stainless-clad steel rod to 350-500 kcmil copper wire. From Table 6, test currents are 1/2 in rod—246 A, 5/8 in rod—285 A, 350 kcmil wire—1441 A, and 500 kcmil wire—1860 A. Select a 5/8 in stainless-clad steel rod and 350 kcmil copper wire and use an initial test current of 285 A,

which should achieve a 350 °C temperature on the stainless-clad steel rod.

*Example 3:* Connector for #1/0-#2/0 copper wire to #4/0-250 kcmil copper wire. From Table 6, test currents are #1/0 wire—620 A, #2/0 wire—725 A, #4/0 wire—1010 A, and 250 kcmil wire—1140 A. Select a #2/0 and #4/0 copper wire and use an initial test current of 725 A, which should achieve a 350 °C temperature on the #2/0 copper wire.

**8.2.2 Test Samples.** Four connectors of each size and type shall be required for each series of sequential tests.

**8.2.3 Equalizer.** Equalizers shall be installed on the stranded conductor on each side of each connector. The equalizer provides an equipotential plane for resistance measurements and prevents the influence of one connection on the other in the current-temperature cycling test. Equalizers are not required on solid conductors.

Any form of equalizer that ensures contact of all strands of a conductor for the duration of the current-temperature cycling test may be used.

When the cables to be joined in a current-temperature cycle loop are identical, a continuous piece of cable may be used between the connections. A short compression sleeve centered between the connections will then act as the equalizer.

NOTE: Resistance measurement points on solid conductors shall be the same as those used for conductors requiring equalizers.

**8.2.4 Conductor Length.** The exposed length of the conductor in the current cycle loop between the connectors and the equalizers shall be as given in Table 4.

**8.3 Ambient Conditions.** The current-temperature cycling tests shall be conducted in a space free of drafts at an ambient temperature of 20 °C (68 °F) to 40 °C (104 °F).

**8.4 Control Conductor.** A control conductor, used for the purpose of obtaining conductor temperature, shall be installed in the current cycle loop between two equalizers. It shall be of the same type and size as the conductor, of those joined by the connector under test, that established the highest temperature. Its length between equalizers shall be the same as the test samples.



**Table 4**  
**Conductor Length from Connector to Equalizer**

Copper Wire or Cable Size AWG or kcmil	Aluminum Wire or Cable Size AWG or kcmil	Steel or Clad Steel Wire or Rod Diameter (in)	Current-Temperature Cycling Test Minimum Conductor Length Exposed from Connector to Equalizer	
			(in)	(mm)
Up to 20	Up to 40	Up to 7/16	12	300
Over 20 to 500	Over 40 to 795	Over 7/16 to 3/4	24	600
Over 500	Over 795	Over 3/4	36	900

**8.5 Current Cycling**

**8.5.1 Current Cycling Period.** Each cycle of the current-temperature cycling test shall consist of maintaining the minimum temperature specified in Table 5 on the control conductor for one hour and then cooling to room ambient. For suggested test currents, refer to Table 6.

**8.5.2 Number of Cycles.** The connections shall be subjected to a minimum of 25 current cycles.

**8.5.3 Current Cycling Temperature.** The current shall be adjusted over the first five cycles to result in a steady-state temperature on the control conductor specified in Table 5, and adjusted every five cycles thereafter as required to attain the specified steady-state temperature for a total of 25 cycles.

**8.6 Loop Configuration.** Loop configuration shall provide a minimum space of 2 ft (610 mm) between the connected conductor, 2.5 ft (760 mm) from the floor, 4 ft (1220 mm) from the ceiling, and 2 ft (610 mm) from the walls.

The current cycle loop may be bent back on itself in a U or zigzag shape provided the above spacings are used.

**Table 5**  
**Conductor Temperature**

Conductor	Temperature for Current Cycling Test
Aluminum	250 °C
Copper	350 °C
Steel	350 °C
Copper-clad steel	350 °C
Galvanized steel	250 °C
Stainless steel	350 °C
Stainless-clad steel	350 °C

**8.7 Measurements.** Resistance and temperature measurements shall be recorded at the beginning of the test and after every five cycles.

**8.7.1 Resistance Measurements.** Resistance measurements shall be made during the current-off period and when the conductor temperature has stabilized at ambient. The measurements shall be made across each connector between potential points located in the center of the equalizers adjacent to the connector or at the equivalent points on a solid conductor. For these measurements, a current of a sufficiently low magnitude shall be used to avoid appreciable heating.

**8.7.2 Temperature Correction.** Ambient temperature shall be recorded concurrently with each set of resistance measurements, and the resistance shall be corrected to 20 °C. The corrected resistance shall be used in evaluating the performance of the connection.

**8.7.3 Temperature Measurements.** Temperature measurements shall be recorded for the connectors and the control conductor near the end of the current heating period, with current on. The temperature shall be measured by means of thermocouples permanently installed on each connector as close as possible to the point in the current path midway between the two conductors. One thermocouple shall be installed at the midpoint of the control conductor.

**9. Freeze-Thaw Test**

**9.1 General.** This test is intended to assure the conformance to resistance criteria of connections subjected to repeated cycles of freezing and thawing in water.