

## PENTAIR 4-POST RACK

DES. **J. ROBERSON**

JOB NO. **11-1461**

DATE **6/24/15**

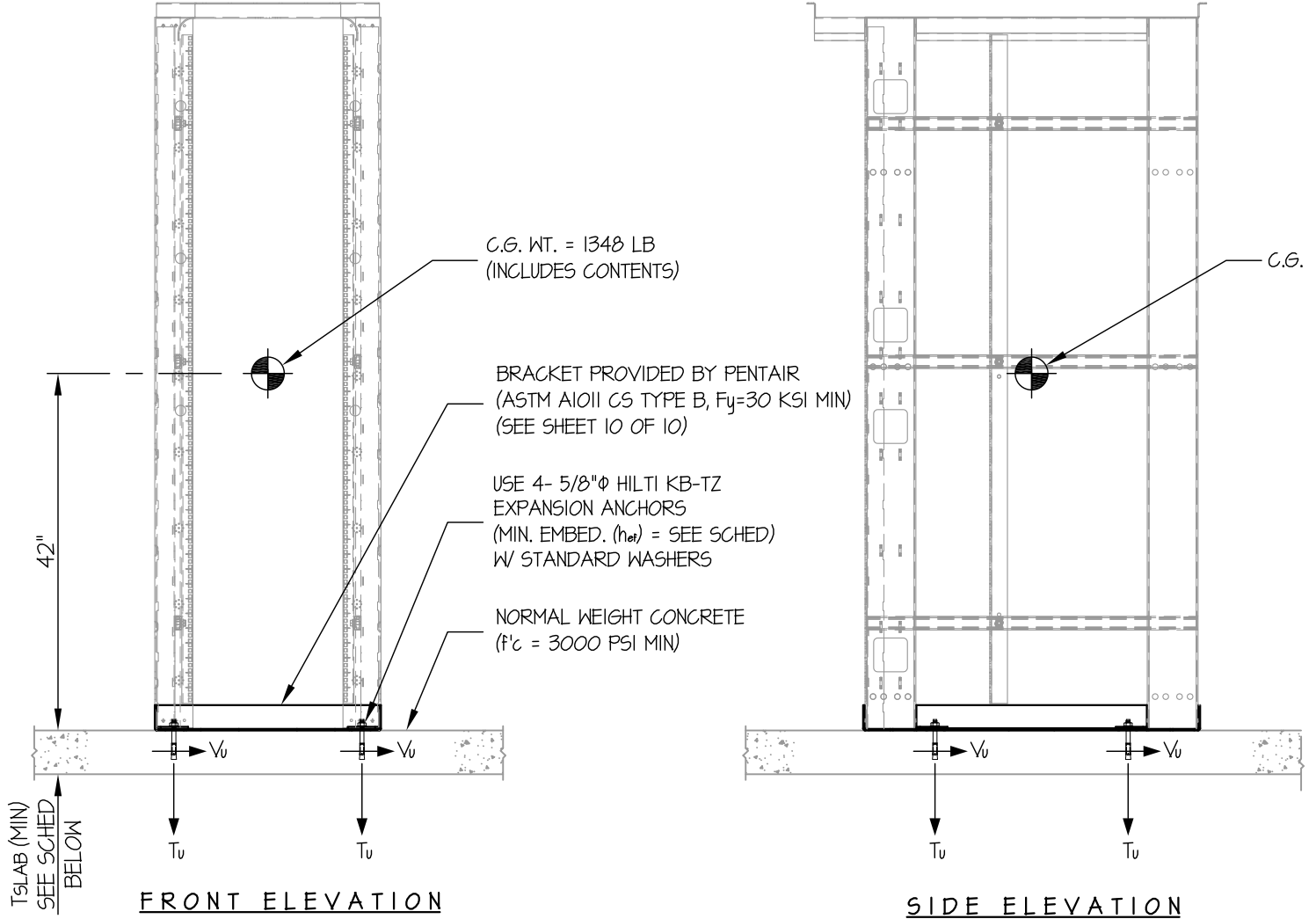
SHEET

**4**

OF **10** SHEETS

SEISMIC SUPPORTS & ATTACHMENTS

CONCRETE SLAB



MAX Sds	ANCHORS			QTY	T <sub>SLAB</sub>	* T <sub>u</sub>	* V <sub>u</sub>	DETAIL
	TYPE	DIAM	EFF EMBED					
150	HILTI KB-TZ	5/8"	3.125"	4	5"	2208	570	SHEET 5 OF 10
220	HILTI KB-TZ	5/8"	4"	4	6"	3382	836	SHEET 6 OF 10

\* VALUES INCLUDE  $\Omega_0$

**NOTES:**

- FORCES ARE DETERMINED PER 2013 CALIFORNIA BUILDING CODE AND ASCE 7-10. STRENGTH DESIGN IS USED. ( $\alpha_p = 2.5, l_p = 1.5, R_p = 6.0, \Omega_0 = 2.5, z/h = 0$ )
- CENTER OF GRAVITY (C.G.) AND WEIGHT ARE THE GOVERNING PARAMETERS FOR DESIGN. THIS PREAPPROVAL ENCOMPASSES ALL WEIGHTS UP TO THE MAXIMUM WEIGHT SHOWN.
- STRUCTURAL ENGINEER OF RECORD FOR THE BUILDING SHALL PROVIDE SUPPORT STRUCTURE DESIGNED TO SUPPORT WEIGHTS AND FORCES SHOWN IN COMBINATION WITH ALL OTHER LOADS THAT MAY BE PRESENT.



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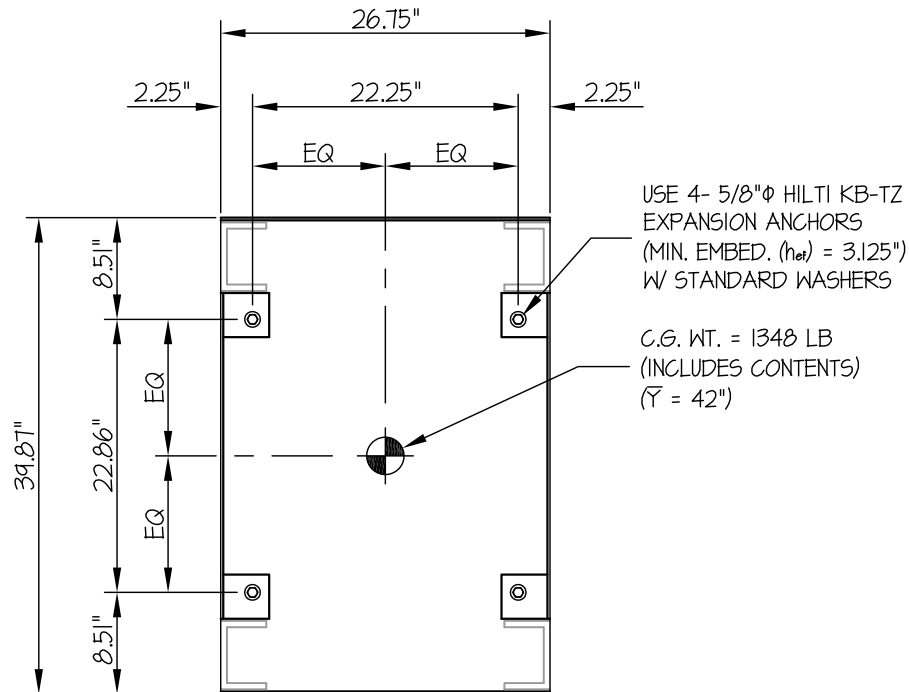
**5**

OF **10** SHEETS

SEISMIC SUPPORTS & ATTACHMENTS

MAX Sds ≤ 150

CONCRETE SLAB



PLAN AT BASE

LOADS: PER 2013 CALIFORNIA BUILDING CODE AND ASCE 7-10.

STRENGTH DESIGN IS USED (S<sub>ds</sub> = 150, a<sub>p</sub> = 2.5, I<sub>p</sub> = 15, R<sub>p</sub> = 6.0, Ω<sub>o</sub> = 2.5, z/h = 0)

WEIGHT = 1348 LB

HORIZONTAL FORCE (E<sub>mh</sub>) = 169W<sub>p</sub> = 2278 LB

VERTICAL FORCE (E<sub>v</sub>) = 0.30W<sub>p</sub> = 404 LB

BOLT FORCES:

BOLT SPECS: 5/8"φ HILTI KB-TZ (h<sub>ef</sub> = 3.125")

φT = 0.75φN<sub>n</sub> = 2508 LB/BOLT (TENSION)

φV = φV<sub>n</sub> = 4940 LB/BOLT (SHEAR)

TENSION (T)

$$T_{u \text{ MAXIMUM}} = \left[ \frac{2278\#(42")}{2 \text{ BOLTS } (31.37")} \times (0.3) \right] + \frac{2278\#(42")}{2 \text{ BOLTS } (24.5")} - \frac{1348\#(0.9) - 404\#}{4 \text{ BOLTS}} = 2208 \text{ LB/BOLT (MAX)}$$

( HORIZ - SIDE TO SIDE )                      ( HORIZ - FRONT TO BACK )                      ( WEIGHT(0.9) - E<sub>v</sub> )

SHEAR (V)

$$V_{u \text{ MAXIMUM}} = \frac{2278\#}{4 \text{ BOLTS}} = 570 \text{ LB/BOLT (MAX)}$$

UNITY CHECK:

$$\left( \frac{T_u}{\phi T} \right) + \left( \frac{V_u}{\phi V} \right) \leq 1.2 \left( \frac{2208}{2508} \right) + \left( \frac{570}{4940} \right) = 1.00 \leq 1.2 \therefore \text{O.K.}$$

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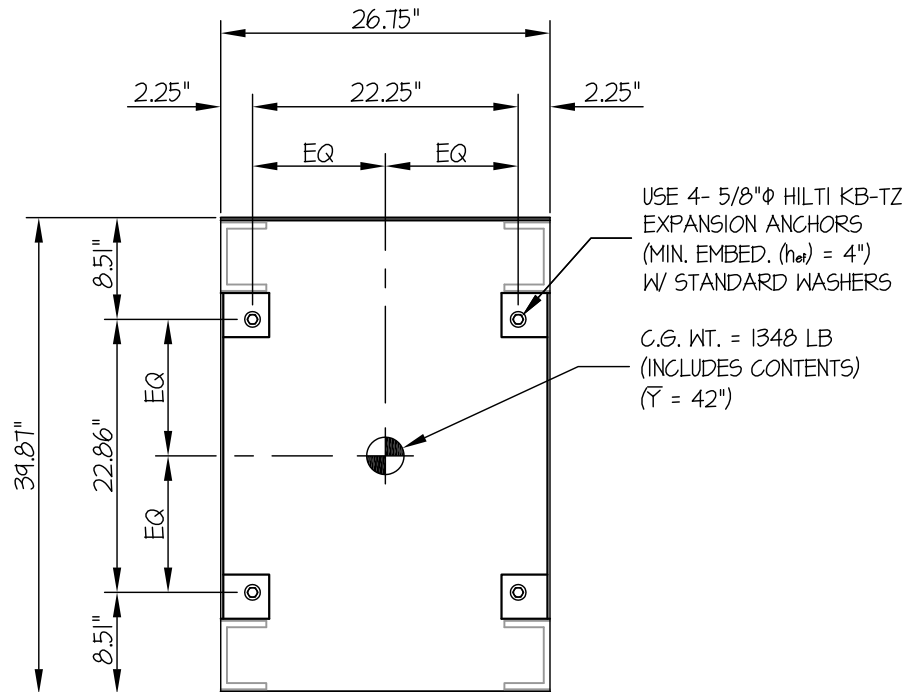
**6**

OF **10** SHEETS

SEISMIC SUPPORTS & ATTACHMENTS

1.50 < MAX S<sub>ds</sub> ≤ 2.20

CONCRETE SLAB



PLAN AT BASE

LOADS: PER 2013 CALIFORNIA BUILDING CODE AND ASCE 7-10.

STRENGTH DESIGN IS USED (S<sub>ds</sub> = 2.20, a<sub>p</sub> = 2.5, I<sub>p</sub> = 15, R<sub>p</sub> = 6.0, Ω<sub>o</sub> = 2.5, z/h = 0)

WEIGHT = 1348 LB

HORIZONTAL FORCE (E<sub>mh</sub>) = 2.48W<sub>p</sub> = 3343 LB

VERTICAL FORCE (E<sub>v</sub>) = 0.44W<sub>p</sub> = 593 LB

BOLT FORCES:

BOLT SPECS: 5/8"φ HILTI KB-TZ (h<sub>ef</sub> = 4")

φT = 0.75φN<sub>n</sub> = 3632 LB/BOLT (TENSION)

φV = φV<sub>n</sub> = 4940 LB/BOLT (SHEAR)

TENSION (T)

$$T_{u \text{ MAXIMUM}} = \left[ \frac{3343\#(42")}{2 \text{ BOLTS } (31.37")} \times (0.3) \right] + \frac{3343\#(42")}{2 \text{ BOLTS } (24.5")} - \frac{1348\#(0.9) - 593\#}{4 \text{ BOLTS}} = 3382 \text{ LB/BOLT (MAX)}$$

( HORIZ - SIDE TO SIDE )                      ( HORIZ - FRONT TO BACK )                      ( WEIGHT(0.9) - E<sub>v</sub> )

SHEAR (V)

$$V_{u \text{ MAXIMUM}} = \frac{3343\#}{4 \text{ BOLTS}} = 836 \text{ LB/BOLT (MAX)}$$

UNITY CHECK:

$$\left( \frac{T_u}{\phi T} \right) + \left( \frac{V_u}{\phi V} \right) \leq 1.2 \left( \frac{3382}{3632} \right) + \left( \frac{836}{4940} \right) = 1.10 \leq 1.2 \therefore \text{O.K.}$$

## PENTAIR 4-POST RACK

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SHEET

**7**

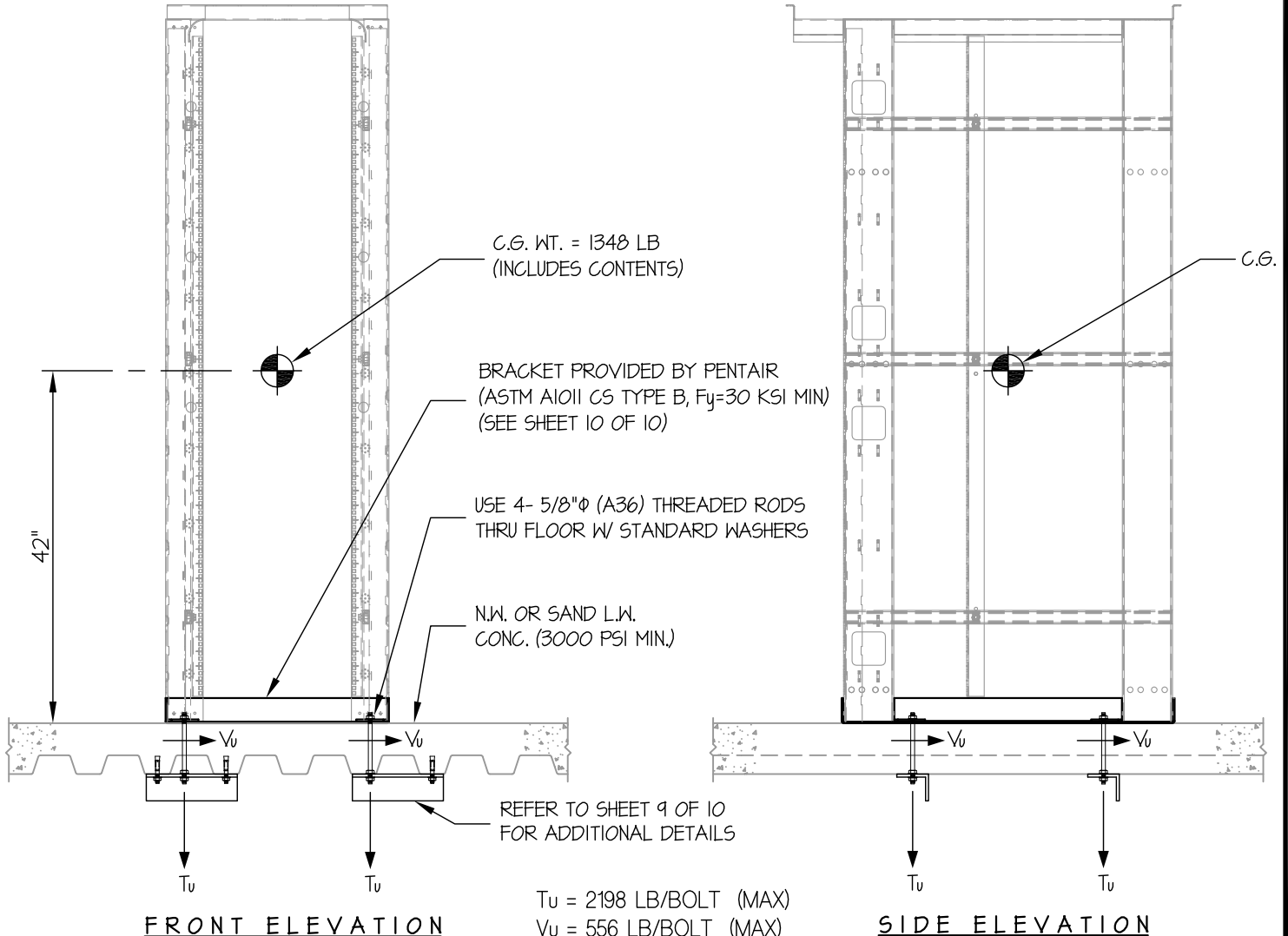
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OF **10** SHEETS

**SEISMIC SUPPORTS & ATTACHMENTS**

**CONCRETE SLAB ON METAL DECK**



**FRONT ELEVATION**

**SIDE ELEVATION**

$T_u = 2198 \text{ LB/BOLT (MAX)}$   
 $V_u = 556 \text{ LB/BOLT (MAX)}$   
(VALUES DO NOT INCLUDE  $\Omega$ )

**NOTES:**

- FORCES ARE DETERMINED PER 2013 CALIFORNIA BUILDING CODE AND ASCE 7-10.**

STRENGTH DESIGN IS USED. ( $S_{Ds} = 2.20$ ,  $a_p = 2.5$ ,  $I_p = 1.5$ ,  $R_p = 6.0$ ,  $\Omega_o = 2.5$ ,  $z/h \leq 1$ )

HORIZONTAL FORCE ( $E_h$ ) =  $1.65 W_p$

HORIZONTAL FORCE ( $E_{mh}$ ) =  $4.13 W_p$  (FOR CONCRETE ANCHORAGE)

VERTICAL FORCE ( $E_v$ ) =  $0.44 W_p$

- CENTER OF GRAVITY (C.G.) AND WEIGHT ARE THE GOVERNING PARAMETERS FOR DESIGN. THIS PREAPPROVAL ENCOMPASSES ALL WEIGHTS UP TO THE MAXIMUM WEIGHT SHOWN.
- STRUCTURAL ENGINEER OF RECORD FOR THE BUILDING SHALL PROVIDE SUPPORT STRUCTURE DESIGNED TO SUPPORT WEIGHTS AND FORCES SHOWN IN COMBINATION WITH ALL OTHER LOADS THAT MAY BE PRESENT.



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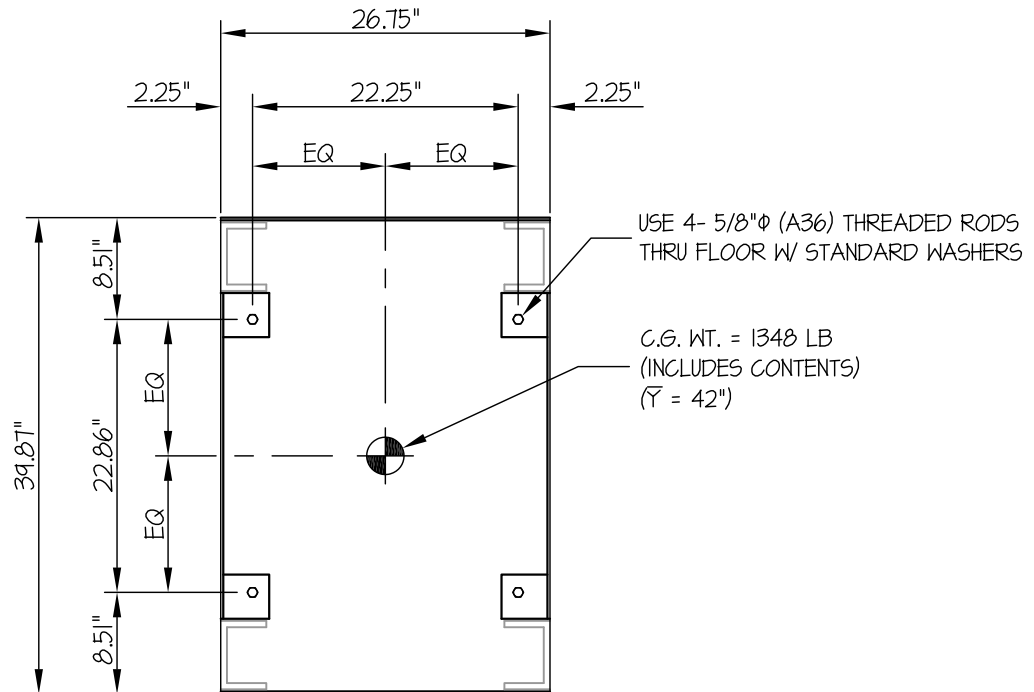
SHEET

**8**

OF **10** SHEETS

SEISMIC SUPPORTS & ATTACHMENTS

CONCRETE SLAB ON METAL DECK



PLAN AT BASE

LOADS: PER 2013 CALIFORNIA BUILDING CODE AND ASCE 7-10.

STRENGTH DESIGN IS USED ( $S_{ds} = 2.20$ ,  $a_p = 2.5$ ,  $I_p = 1.5$ ,  $R_p = 6.0$ ,  $\Omega_o = 2.5$ ,  $z/h \leq 1$ )

WEIGHT = 1348 LB

HORIZONTAL FORCE ( $E_h$ ) =  $1.65W_p = 2224$  LB

HORIZONTAL FORCE ( $E_{mh}$ ) =  $4.13W_p = 5567$  LB

VERTICAL FORCE ( $E_v$ ) =  $0.44W_p = 593$  LB

BOLT FORCES:

BOLT SPECS: 5/8"φ (A36) THREADED ROD

φT = 10,016 LB/BOLT (TENSION)

φV = 5342 LB/BOLT (SHEAR)

TENSION (T)

$$T_{u \text{ MAXIMUM}} = \left[ \frac{2224\#(42")}{2 \text{ BOLTS } (31.37")} \times (0.3) \right] + \frac{2224\#(42")}{2 \text{ BOLTS } (24.5")} - \frac{1348\#(0.9) - 593\#}{4 \text{ BOLTS}} = 2198 \text{ LB/BOLT (MAX)}$$

( HORIZ - SIDE TO SIDE )      ( HORIZ - FRONT TO BACK )      ( WEIGHT(0.9) -  $E_v$  )

SHEAR (V)

$$V_{u \text{ MAXIMUM}} = \frac{2224\#}{4 \text{ BOLTS}} = 556 \text{ LB/BOLT (MAX) (PER AISC J3.7, LESS THAN 20% STRESS)}$$

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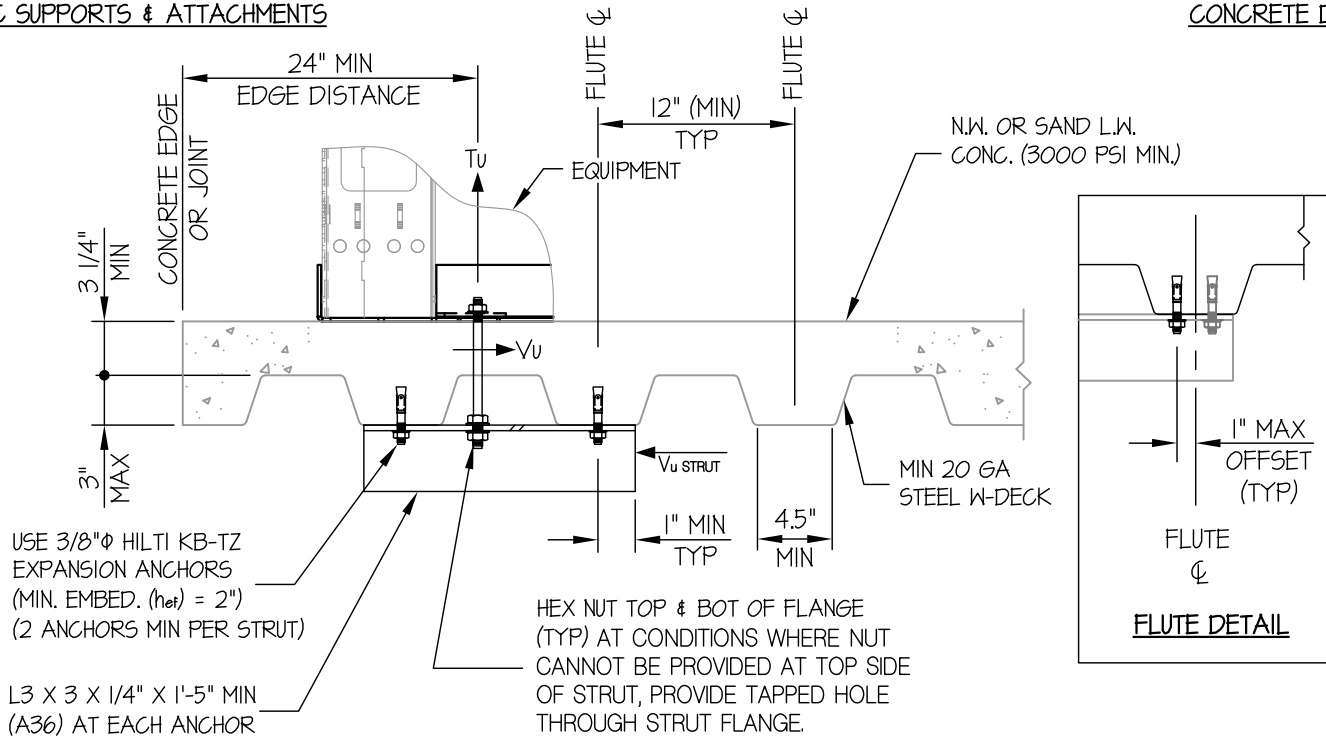
SHEET

**9**

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SEISMIC SUPPORTS & ATTACHMENTS

CONCRETE DETAIL



MIN STEEL DECK REQUIREMENTS AND STRUT DETAIL

DEMANDS: (BASED ON UPPER FLOOR)

$$T_u = 2198 \text{ LB/BOLT}$$

$$V_u = 556 \text{ LB/BOLT}$$

$$V_{u \text{ STRUT}} = 0.7V_u = 0.7(556\#) = 389 \text{ LB/STRUT}$$

CONCRETE ANCHORS AT STRUT

$$V'_u \text{ STRUT} = \Omega_0 V_{u \text{ STRUT}} = 2.5(389\#) = 973 \text{ LB/STRUT}$$

USE 2 BOLTS MIN

$$V'_u \text{ BOLT} = 973\# / (2 \text{ BOLTS}) = 487 \text{ LB/BOLT}$$

BOLT SPEC: 3/8"  $\phi$  HILTI KB-TZ: (h<sub>ef</sub> = 2" MIN)

$$\phi V = 938 \text{ LB/BOLT}$$

STRUT DESIGN (L3 X 3 X 1/4" : S = 0.569 in<sup>3</sup>, A36)

$$M_u \text{ STRUT} = \frac{2198\#(14")}{4} = 7693\#\text{'}$$

$$\frac{b}{t} = \frac{3}{0.25} = 12 \leq 0.54 \sqrt{\frac{E}{F_y}} = 0.54 \sqrt{\frac{29000}{36}} = 15.3$$

$$\begin{aligned} \therefore M_n &= 1.5 F_y S_c \\ &= 1.5(36000)(0.8 \times 0.569) \\ &= 24580\#\text{'} \end{aligned}$$

$$\phi M_n = 0.9 M_n = 0.9(24580\#) = 22123\#\text{'} > 7693\#\text{'}. \therefore \text{O.K.}$$

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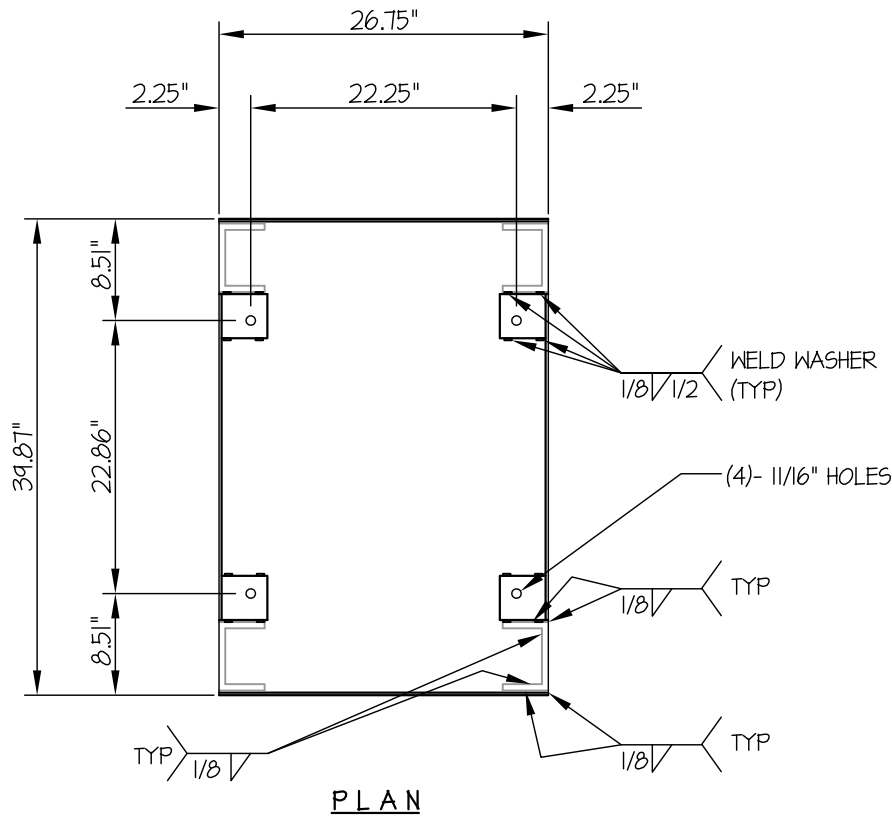
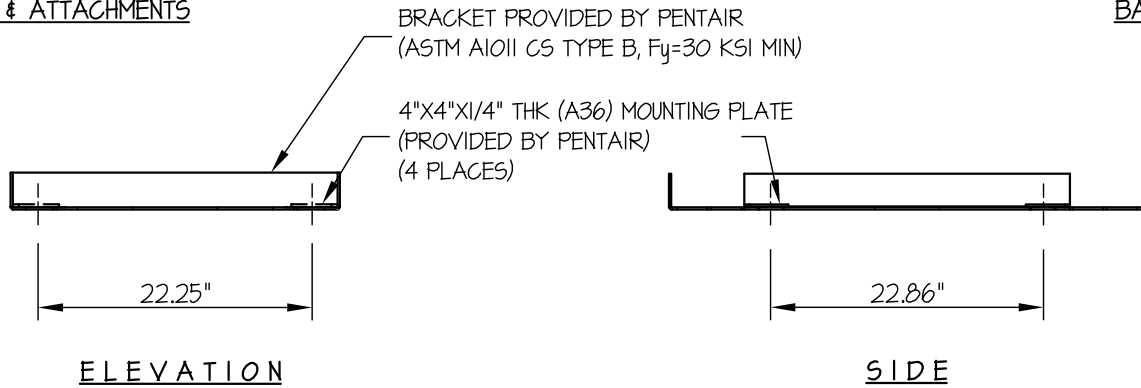
SHEET

# 10

OF **10** SHEETS

SEISMIC SUPPORTS & ATTACHMENTS

BASE DETAIL



LOADS TO BASE: (BASED ON UPPER FLOOR DEMANDS)

$T_u = 2198$  LB/BOLT (NON-PRYING)

$V_u = 556$  LB/BOLT